

## STORMWATER MANAGEMENT REPORT

**FOR** 

Elcon Recycling
Dean Sievers Place
Falls Township
Bucks County, PA

File No. 12-07083

Original Submission: January, 2019

Resubmitted: April 18, 2019

#### Prepared by:

Gilmore & Associates, Inc.
Engineers + Land Surveyors + Planners + GIS Consultants
65 E. Butler Avenue
New Britain, PA 18901
(215) 345-4330

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#### I. Project Description

The subject site (Tax parcel 13-51-1-5) is located in the Materials Processing and Manufacturing (MPM) zoning district. The site is bound by Phoenix Metals, Arley Wholesale, A&A Machinery, and Univar USA along Dean Sievers Place to the east, Sims Metal Management to the north, and Steel Road South to the west and south, in Falls Township. The attached USGS Quadrangle depicts the site location. The 32.30-acre site is currently undeveloped. The site is generally flat, but slopes toward the existing wetland at approximately one (1) percent. The majority of the site currently sheet flows directly to the existing wetland (POI-A), with a small portion of the site sheet flowing to an existing drainage swale along Dean Sievers Place and then to the wetland. The remaining portion of the site sheet flows to an adjacent property, TMP 13-51-1-6 (POI-B). The existing wetland system eventually discharges to the Delaware River, which is classified as WWF, MF in Chapter 93.

The project proposes a network of interconnected buildings covering approximately 107,100 square feet for the purpose of treating industrial waste. An additional ±50,000 square feet within the limit of disturbance has been reserved for future development. This future development area has been considered in the stormwater design, and is included in the calculations as impervious building area. Drive aisles capable of accommodating a WB-67 truck will be provided throughout the site, as well as a designated truck unloading area and a parking area for 73 vehicles. The truck unloading area is graded to be self-contained and will direct runoff collected in this area to the processing plant as an extra precaution against leaks or spills. The process tank farm in the large central island will also be self-contained and direct runoff to be processed. Runoff from area to be disturbed will be directed to one (1) stormwater basin.

#### II. Existing Conditions: Topography & Soils

Topographic information was obtained from a field survey performed by Gilmore & Associates, Inc. in March of 2014. Vertical Datum is NAVD88 and was established by Global Positioning System (GPS) with observations referenced to the TopCon TopSurv GPS Base Station Network.

Soils classification information for the project site was obtained from the Soil Survey of Bucks County, Pennsylvania, and is presented in Table 1. Urban Land (UfuB) is the only soil mapped within the area of disturbance.

Table 1: Existing Soils Classification Table

Symbol	Soil)Name	Rating	Slope
UfuB	Urban Land		0-8%
Na	Nanticoke-Hatboro Silt Loams	C/D	0-1%
W	Water	<u> </u>	

#### III. Stormwater Management

The proposed stormwater management design for this project incorporates both structural and non-structural BMPs. The non-structural BMPs utilized in the design include minimization of the overall disturbed area to the maximum extent possible and limitation of the proposed impervious coverage to only what is needed for the proposed use. Limiting the impervious coverage and overall disturbed area reduces the composite CN value in the postdevelopment condition and reduces runoff. Also, the existing drainage swale between the proposed development and Dean Sievers Place will be maintained to continue to direct offsite runoff to the existing wetland system. Further, a managed release basin with an impermeable liner is proposed to treat the stormwater from the disturbed area. After stormwater enters the basin through one (1) of two (2) endwalls, it will first infiltrate through two (2) feet of amended soils for water quality, then enter the perforated underdrain and slowly discharge through the hole drilled in the capped underdrain in the outlet control structure. The outlet control structure also has a rectangular orifice and grated top to mitigate peak flows in accordance with the Falls Township Stormwater Management Ordinance (Chapter 187). This basin will discharge to the existing wetland system via an endwall with a rip-rap apron sized in accordance with the 2012 PADEP Erosion and Sediment Pollution Control Program Manual. The discharge will then be dispersed over a fifty (50) foot wide level spreader to an area stabilized by existing brush in an effort to reduce the impact to the local wetland environment from a concentration of the site runoff.

PADEP has requested that infiltration not be included in the stormwater management design for this project. As such, an impermeable liner will be installed below the underdrain in the proposed basin to fully contain all runoff from the disturbed area.

The stormwater management design is based on the Soil Conservation Service (SCS) Method for runoff peak flow rates and volumes utilizing the Hydraflow Hydrographs computer software program. The proposed stormwater conveyance system design is based on the Rational Method utilizing the Hydraflow Storm Sewers computer software program. All inlets, storm sewer pipes, and the proposed stormwater basin have been designed to contain and convey the 100 year storm, exceeding standards set forth in the Falls Township Stormwater Management Ordinance (Chapter 187). Time of concentration calculations for the stormwater management design are attached. In order to comply with the ACT 167 Plan, the above stormwater management design criteria are based on the Falls Township Stormwater Management Ordinance (Chapter 187) adopted April 5, 2005.

### A. Peak Flow Rate Analysis per §187-9(A)(2)

This site is located within District C, which requires post-development runoff rate control as follows:

District	Post-Development		Pre-Development
	Design Storm		Design Storm
	2-year	reduced to	1-year
С	5-year	reduced to	2-year
	100-year	reduced to	50% of 100-year

Runoff rate will be controlled in accordance with the requirements above per the following table:

Table 2: Runoff Peak Discharge Rate Summary (cfs)

Gondition	1-year	2-year	5-year	10-year	25-year	50-year	100-year
Pre-Development POI-A	4.80	8.54	15.00	21.32	28.06	33.33	40.55
Pre-Development POI-B	1.15	2.04	3.57	5.07	6.66	7.91	9.62
Post-Development POI-A	2.03	3.09	4.84	7.28	10.38	12.30	14.75
Post-Development POI-B	0.19	0.29	0.45	0.61	0.78	0.91	1.08

### B. Water Quality Analysis per §187-17

The Falls Township Stormwater Management Ordinance requires that 90% of the average annual rainfall be treated over the developed portions of the site per the following equation:

$$WQv = [(P) \times (Rv) \times (A)] \div 12$$

Where:

WQv = water quality volume (acre-feet)

P = rainfall amount equal to 90% of events producing this rainfall (inches)

P = 2.04 inches for PennDOT Region 5

A = area of project contributing to the water quality BMP (acres)

 $Rv = 0.05 + [0.009 \times (I)]$  where I is the percent of the area that is impervious surface

(impervious area  $\div$  A × 100%)

The required WQv for this site is:

$$WQv = [(P) \times (Rv) \times (A)] \div 12$$

$$Rv = 0.05 + [0.009 \times (I)]$$

 $I = impervious area \div A \times 100\%$ 

$$I = 8.09 \div 13.40 \times 100\%$$

I = 60.4

$$Rv = 0.05 + [0.009 \times 60.4]$$

$$Rv = 0.59$$

$$WQv = [(2.04 in) \times (0.59) \times (13.40)] \div 12$$

$$WQv = 1.34 \text{ acre-feet} = 58,370 \text{ cf}$$

The WQv provided by the managed release basin is equal to the volume that flows to the basin and stays below the lowest basin outlet invert. This volume will infiltrate through the amended soils in the managed release basin to achieve the required water quality and discharge through the orifice in the underdrain located in the outlet control structure. Since

the maximum water surface for the 2-year storm is below the lowest orifice invert, the entire runoff volume for the 2-year storm that is directed to the managed release basin will be treated to the required water quality. The runoff volume from the 2-year storm event that flows to the basin is 94,641 cubic feet per the Soil Conservation Service (SCS) Method utilized by the Hydraflow Hydrographs computer software program.

### 94,641 cubic feet provided > 58,370 cubic feet required

### C. Analysis of Dean Sievers Place Channel

There are two (2) crossings proposed across the existing channel in the drainage easement adjacent to Dean Sievers Place. The existing and proposed drainage area and Rational Method coefficient were calculated for each proposed culvert crossing, see attached exhibits and Rational Method coefficient calculations. As shown in the attached Hydraflow Hydrographs computations, the proposed condition results in less runoff to the proposed headwall locations.

#### IV. Erosion and Sediment Control

The following measures shall be implemented to minimize erosion and sediment pollution created by site construction:

- A. Stabilized Construction Entrance(s) Temporary construction entrances will provide stable access routes to the site, and will aid in cleaning mud from vehicle tires during ingress and egress to and from the site.
- B. Compost Filter Socks Compost filter socks will be used to filter sediment from small overland (sheet) flow areas and along the toe of slope of soil stockpiles. Rock filter outlets shall be implemented by the Contractor in low points along the compost filter socks where concentrated flow can occur.
- C. Inlet Protection Installation of inlet protection devices shall be utilized to protect the existing inlets and proposed inlets from receiving increased sediment loads due to construction related activities.
- D. Temporary Seeding and Mulching Disturbed areas which will be "unworked" shall immediately receive a temporary seed mixture and mulch as shown on the plan. In addition, soil stockpile areas are to be seeded and mulched with a temporary seed

mixture to promote rapid vegetated stabilization.

- E. Permanent Seeding and Mulching Disturbed areas at final grade are to receive a permanent seed mixture and mulch to promote permanent stabilization as shown on the plan.
- F. Limited Area of Disturbance No site clearing or grading is proposed which is not essential to the construction of the project. Significant open space areas of the site will remain undisturbed.

#### V. Maintenance

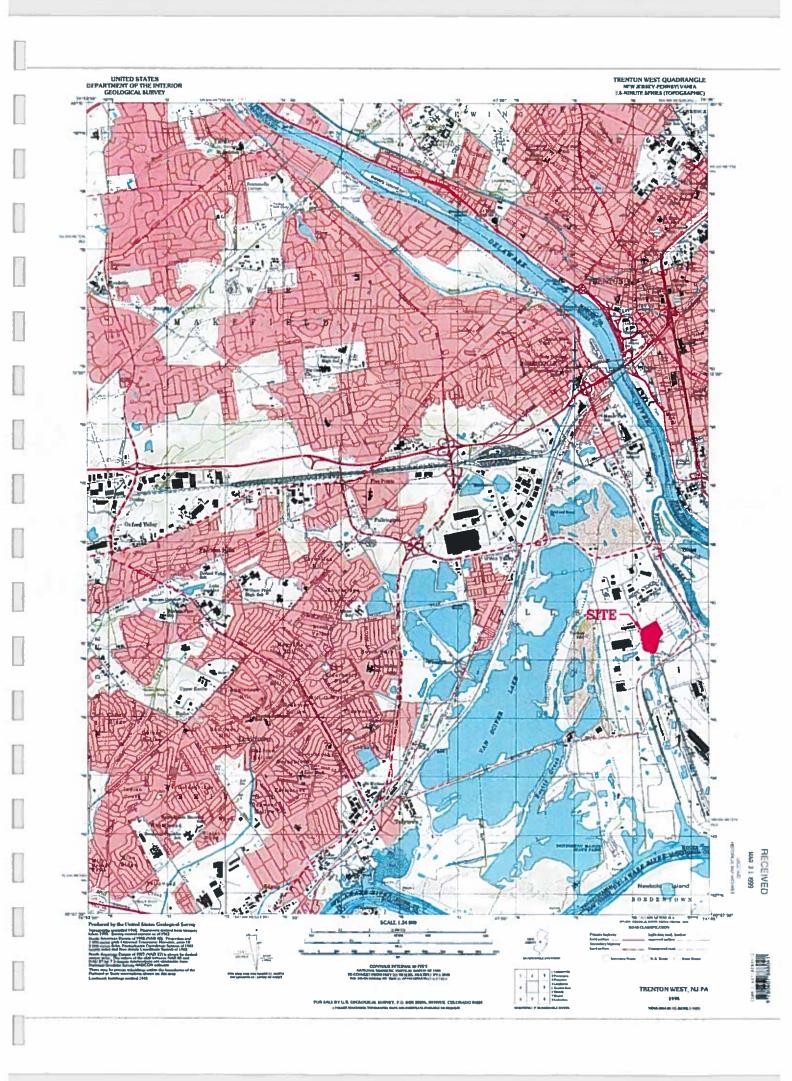
The Owner of the Dean Sievers Place site shall maintain the stormwater management system. Maintenance shall include removal of debris from all inlet locations, as well as removal of any obstructions that may enter the stormwater basin. Falls Township shall also reserve the right to enter the site for the purpose of inspection of these facilities to ensure that the Owner is maintaining the design integrity.

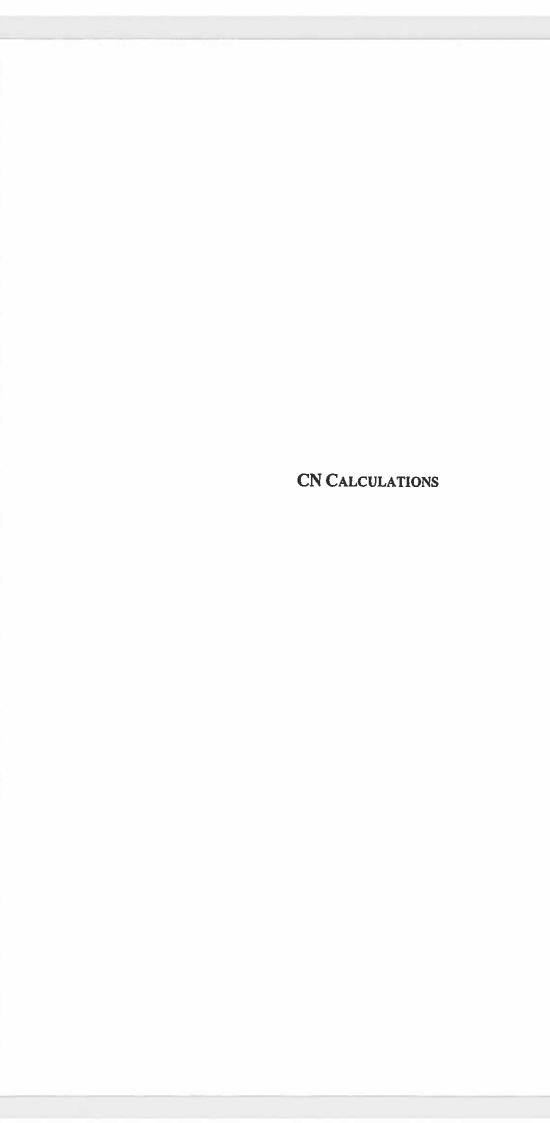
#### VI. Qualifications:

The design of the stormwater management facilities has been completed by James Hersh, P.E. of Gilmore & Associates, Inc. The firm has completed numerous stormwater management projects in Bucks County since 1973.

APPENDIX

USGS QUADRANGLE





**Elcon Recycling** 

**Project Number** 

12-07083

Condition

Pre-Development

Area

On-Site Drainage Area A (Drainage Area to POI-A)

Description	CN	SF	Α	RCN x A
Impervious	98	0	0.00	0
Gravel (HSG-C)	89	0	0.00	0
Brush (HSG-C)	65	88,288	2.03	132
Meadow (HSG-C)	71	392,147	9.00	639
Grass (HSG-C)	74	0	0.00	0
Forest (HSG-C)	70	0	0.00	0
TOTAL		480,435	11.03	771

RCN 70

Time of Concentration : Use Tc = 26.81 min

Elcon Recycling

**Project Number** 

12-07083

Condition

Area

Pre-Development
On-Site Drainage Area B (Drainage Area to POI-B)

Description	CN	SF	Α	RCN x A
Impervious	98	0	0.00	0
Gravel (HSG-C)	89	0	0.00	0
Brush (HSG-C)	65	10,304	0.24	15
Meadow (HSG-C)	71	93,377	2.14	152
Grass (HSG-C)	74	0	0.00	0
Forest (HSG-C)	70	0	0.00	0
TOTAL		103,681	2!38	168

RCN 70

Time of Concentration : Use Tc = 23.11 min

**Elcon Recycling** 

**Project Number** 

12-07083

Condition

Post-Development

Агеа

On-Site Drainage Area A (Drainage Area to Basin)

Description	CN	SF	Α	RCN x A
Impervious	98	349,168	8.02	786
Gravel (HSG-C)	89	0	0.00	0
Brush (HSG-C)	65	0	0.00	0
Meadow (HSG-C)	71	0	0.00	0
Grass (HSG-C)	74	115,360	2.65	196
Forest (HSG-C)	70	Ö	0.00	0
TOTAL		464,528	10.66	982

92

Time of Concentration : Use Tc = 7.97 min

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**Project Number** 

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Condition

Post-Development

Area

On-Site Drainage Area A (Drainage Area to Bypass Basin)

Description	CN	SF	Α	RCN x A
Impervious	98	2,873	0.07	6
Gravel (HSG-C)	89	0	0.00	0
Brush (HSG-C)	65	0	0.00	0
Meadow (HSG-C)	71	0	0.00	0
Grass (HSG-C)	74	110,071	2.53	187
Forest (HSG-C)	70	0	0.00	0
TOTAL		112,944	2.59	193

RCN 75

Time of Concentration : Use Tc = 23.77 min

**Elcon Recycling** 

**Project Number** 

12-07083

Condition

Post-Development

Area

On-Site Drainage Area B (Drainage Area to POI-B)

Description	CN	SF	Α	RCN x A
Impervious	98	0	0.00	0
Gravel (HSG-C)	89	Ō	0.00	0
Brush (HSG-C)	65	0	0.00	0
Meadow (HSG-C)	71	0	0.00	(0)
Grass (HSG-C)	74	6,643	0.15	111
Forest (HSG-C)	70	0	0.00	0
TOTAL		6,643	0.15	i i

RCN 74

Time of Concentration : Use Tc = 5.00 min



Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No. 1

Pre-Dev POI-A

<u>Description</u>	A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.30 = 1.00		0.011 0.0 3.30 0.00		0.011 0.0 3.30 0.00		
Travel Time (min)	= 18.54	+	0.00	+	0.00	=	18.54
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 800.00 = 1.00 = Unpave = 1.61	d	0.00 0.00 Unpave 0.00	ed	0.00 0.00 Unpav	ed	
Travel Time (min)	= 8.26	+	0.00	+	0.00	=	8.26
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 0.00 = 0.00 = 0.00 = 0.015 = 0.00 = 0.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No. 2
Pre-Dev POI-B to TMP 13-51-1-6

<u>Description</u>	A		<u>B</u>		<u>c</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.30 = 0.80		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 20.27	+	0.00	+	0.00	=	20.27
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 230.00 = 0.70 = Unpave = 1.35	d	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 2.84	+	0.00	+	0.00	=	2.84
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 0.00 = 0.00 = 0.00 = 0.015 = 0.00 = 0.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							23.11 mir

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No. 3

Post-Dev to Basin Page 1

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.150 = 20.0 = 3.30 = 2.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 2.66	+	0.00	+	0.00	=	2.66
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 100.00 = 1.10 = Paved = 2.13		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.78	+	0.00	+	0.00	=	0.78
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 1.23 = 3.90 = 0.50 = 0.015 = 3.24 = 286.0		1.77 4.71 0.50 0.015 3.65 317.0		3.14 6.28 0.50 0.015 4.41 139.0		
Travel Time (min)	= 1.47	+	1.45	+	0.52	=	3.44
Total Travel Time, Tc		••••••	**************	•••••	••••••		6.89 min

**Hyd. No. 3**Post-Dev to Basin Page 2

<u>Description</u>	<u>A</u>		<u>B</u>		<u>c</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.150 = 0.0 = 0.00 = 0.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 0.00 = 0.00 = Paved = 0.00		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 4.91 = 7.85 = 0.50 = 0.015 = 5.13 = 80.0		7.07 9.42 0.50 0.015 5.80 286.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.26	+	0.82	+	0.00	=	1.08
Total Travel Time, Tc		••••••	•••••••	••••••	••••••	:	1.08 min + 6.89 min 7.97 min

Hyd. No. 5

Post-Dev to Bypass Basin

<u>Description</u>	A	<u>B</u>	<u>c</u>	<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 80.0 = 3.30 = 1.00	0.011 0.0 0.00 0.00	0.011 0.0 0.00 0.00	
Travel Time (min)	= 15.51 +	0.00 +	0.00 =	15.51
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 800.00 = 1.00 = Unpaved = 1.61	0.00 0.00 Unpaved 0.00	0.00 0.00 Paved 0.00	
Travel Time (min)	= 8.26 +	0.00 +	0.00 =	8.26
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 0.00 = 0.00 = 0.00 = 0.015 = 0.00 = 0.0	0.00 0.00 0.00 0.015 0.00	0.00 0.00 0.00 0.015 0.00	
Travel Time (min)	= 0.00 +	0.00 +	0.00 =	0.00
Total Travel Time, Tc		*************************	***********	23.77 min

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No. 7
Post-Dev POI-B to TMP 13-51-1-6

<u>Description</u>	A	<u> </u>	<u>B</u>		<u>c</u>	<u>Totals</u>	
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0. = 20 = 3. = 33	0.0 .30	0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 1	.26 +	0.00	+	0.00	=	1.26
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 50 = 4. = U: = 3.	.00 npaved	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.	.26 +	0.00	+	0.00	=	0.26
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 0. = 0. = 0. = 0. = 0.	.00 .00 .015 .00	0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00		
Travel Time (min)	= 0.	.00 +	0.00	+	0.00	=	0.00
Total Travel Time, Tc	••••••	*************		•••••	***********		1.52 min





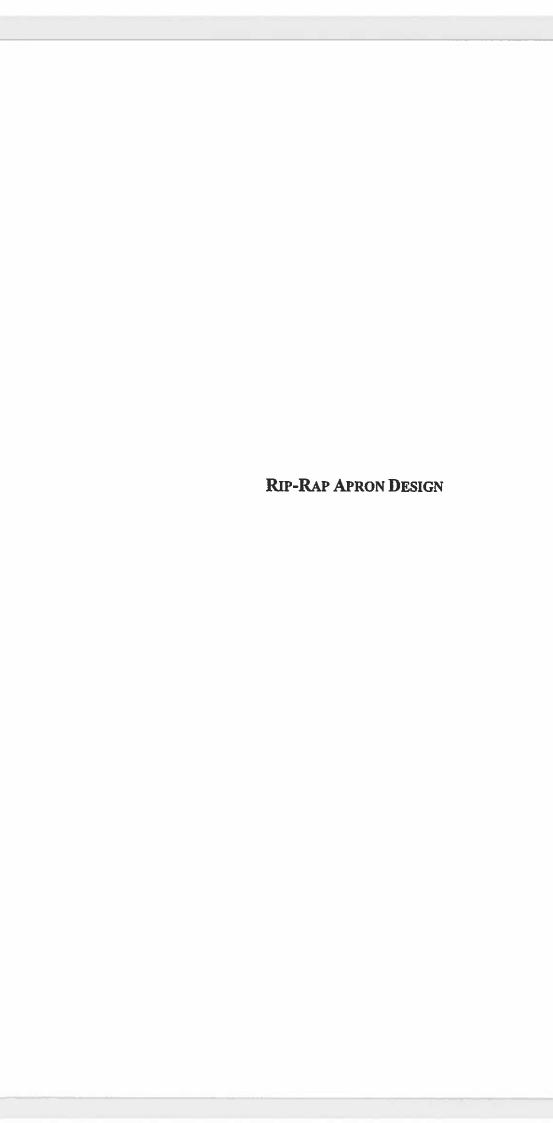
Project Name: Project Number:

Elcon Recycling 12-07083

**BMP Emergency Spillway Calculations** 

 $Q = CLH^{3/2}$ C = 3.10

Impermeable-Line Managed Release Basin	BMP
1573	100-YR DWE
17.75	TOP OF BERM ELEVATION
16.25	100-YR TOP OF BERM EMER. SPILLWAY EMER. SPILLWAY EMER. SPILLWAY DWE ELEVATION WIDTH (FT.) TOP WIDTH (FT.)
90	EMER. SPILLWAY WIDTH (FT.)
99	TOP WIDTH (FT.)
96/24	Q <sub>100</sub>
0,49	H (FT.)
16#74	MAX. WSEL (FT.)
1.01	FREEBOARD SIDI
ω ::	SLOPE



#### **EROSION AND SEDIMENT CONTROL PLAN**

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1

### STANDARD WORKSHEET Rip-Rap Apron Outlet Protection

PROJECT NAME:		Elcon Recycling		
LOCATION:	Falls Township	···		
PREPARED BY:	MRZ	DATE:	4/15/2019	
CHECKED BY:	JJH	DATE:	4/15/2019	

#### **METHODOLOGY:**

Utilize PA D.E.P. Erosion and Sediment Control Manual to construct a Rock Apron at culvert, endwall, headwall or channel outfalls. First, tailwater condition must be determined (minimum or maximum). Second, with a known discharge, determine D50 rock size and length of apron "La". Third, determine the width and thickness of the apron. Lastly, ensure the permissible velocity of the rock size chosen is not exceeded by the velocity of the discharge entering the apron.

#### **Equations Utilized:**

Minimum Tailwater Condition: W2 = 3do + La Maximum Tailwater Condition: W2 = 3do + 0.4La

Blanket Thickness: T = 1.5\*Dmax

Discharge (Q) and Velocity (V) - obtained from the 100 Year Storm

do = pipe diameter

Width 1 = initial width of apron at end of structure

Width 2 = terminal width of apron, W2

Flows from Hydraflow Computations

		STRUC	TURE D	ATA	/		RIP-RAP DATA				APRON DAT	ГА
TYPE#	PIPE DIA.	Tailwtr Cond.	Mngs	Pipe Slope	d	V	D50	ROCK	Rock T	La	W at pipe	W at tailwtr
	(in)	MIN/MAX	"	(ft/ft)	(cfs)	(fps)	(in.)	SIZE	(in.)	(ft)	(ft)	(ft)
EW-1	36.0	MIN	0.015	0.005	36.14	5.11	6	R-4	18	19	9	28
EW-2	18.0	MIN	0.015	0.005	7.36	4.16	3	R-3	9	9	4.5	13.5
EW-3	15.00	MIN	0.015	0.005	10.92	8.90	6	R-4	18	13	3.75	16.75
								R-7	0		0	0
			(X)					R-7	0		0	0
								R-7	0		0	0
								R-7	0	<u> </u>	0	0
								R-7	0		0	0
								R-7	0		0	0

Note: Rock size selected has been increased from the suggested d50 values based upon flow (Q) and/or velocity parameters. Energy Dissipator shall be hand placed and dimensions adjusted to conform to the existing roadside conveyance.

Stone larger than R-4 shall have stone filter blanket installed prior to the rip-rap in lieu of non-woven geotextile. Filter stone shall meet the following requirements:

Rip-rap		Filter Blanket Requirements									
Gradation	depth	stone#	d50	min.							
R-5	6"	FS-2	2"	no. 4	по. 100						
R-6	8"	FS-3	6.5"	2.5"	no. 16						
R-7	10"	FS-3	6.5"	2.5*	no. 16						

TABLE 6.6

Riprap Gradation, Filter Blanket Requirements, Maximum Velocities

			assing (Squar		num Velocitie	
Class, Size NO.						
Rock Size (Inches)	R-8	R-7	R-6	R-5	R-4	R-3
42	100					
30		100				
24	15-50		100			
18		15-50		100		
15	0-15					
12		0-15	15-50		100	
9				15-50		
6			0-15		15-50	100
4				0-15	""	
3					0-15	15-50
2						0-15
Nominal Placement Thickness (inches)	63	45	36	27	18	9
Filter Stone <sup>1</sup>	AASHTO #1	AASHTO #1	AASHTO #1	AASHTO #3	AASHTO #3	AASHTO #57
V <sub>max</sub> (ft/sec)	17.0	14.5	13.0	11.5	9.0	6.5

Adapted from PennDOT Pub. 408, Section 703.2(c), Table C

1 This is a general standard. Soil conditions at each site should be analyzed to determine actual filter size. A suitable woven or non-woven geotextile underlayment, used according to the manufacturer's recommendations, may be substituted for the filter stone for gradients < 10%.

TABLE 6.7
Comparison of Various Gradations of Coarse Aggregates

	Total Percent Passing														
AASHTO NUMBER	6 1/2	4"	3 1/2"	2 1/2	2"	1 1/2 "	1"	3/4 "	1/2"	3/8"	:#4	#8	#16	#30	#100
1		100	90-100	25-60		0-15		0-5							
3				100	90-100	35-70	0-15	1	0-5						
5						100	90-100	20-55	0-10	0-5					
57						100	90-100		25-60		0-10	0-5			
67							100	90-100		20-55	0-10	0-5			
7								100	90-100	40-70	0-15	0-5			
8					ľ				100	85-100	10-30	0-10	0-5		
10										100	75-100				10-30

PennDOT Publication 408, Section 703.2(c), Table C

Tables 6.6 and 6.7 should be placed on the plan drawings of all sites where riprap channel linings are proposed.

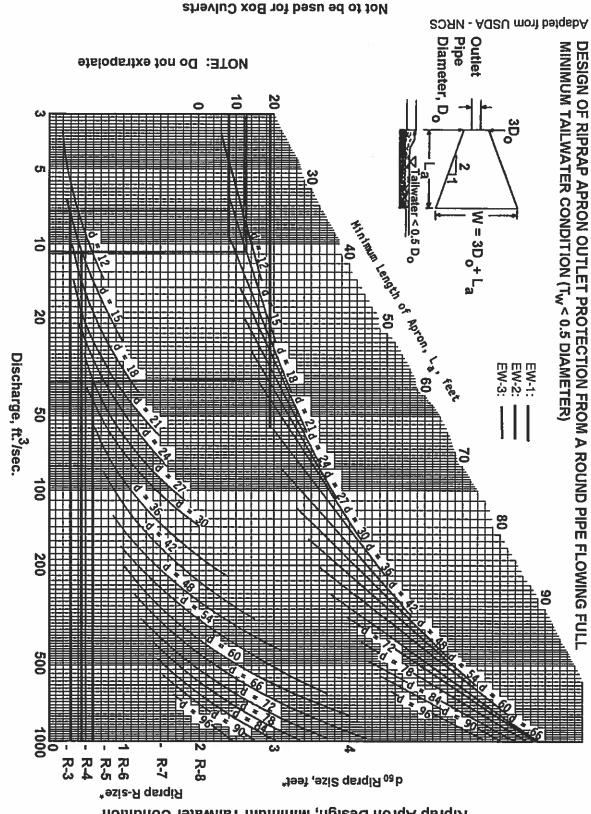
TABLE 6.9
Recommended n Values to be Used with Manning's Equation When Doing Stability
Analyses of Receiving Streams

# <u>Design values should be utilized unless documentation is provided</u> (narrative/calculations) to show that another value within the minimum and maximum range is appropriate.

Surface	Min.	Design	Max.
Asphalt Lining		0.015	
Brick in cement mortar; brick sewers	0.012	0.015	0.017
Concrete-lined channel	0.012	0.015	0.018
Cement-rubble surface	0.017		0.030
Neat cement surfaces	0.010	0.012	0.013
Plastic-lined channel	0.012		0.014
Shotcrete	0.016	Yı.	0.017
Asbestos Cement Pipe		0.009	
Concrete pipe	0.012	0.015	0.016
Vitrified Clay Pipe	0.010	0.013	0.017
Common-clay drainage tile	0.011	0.012	0.017
Semi-circular metal flumes, smooth	0.011		0.015
Corrugated	0.023	0.025	0.030
Channels and ditches			
Earth, straight and uniform	0.017	0.023	0.025
Rock cuts, smooth and uniform	0.025	0.030	0.035
jagged and irregular	0.035	0.040	
Dredged earth channels	0.025	0.028	0.033
Earth bottom, rubble sides	0.028	0.030	0.035
Natural Streams			<del>-</del>
Clean, straight bank, full stage no rifts or deep pools	0.025		0.033
2. Same as 1, but some weeds and stones	0.030		0.040
3. Winding, some pools and shoals, clean	0.033		0.045
Same as 3, lower stages, more ineffective slope and sections	0.040		0.055
5. Same as 3, same weeds and stone	0.035		0.050
6. Same as 4, stony sections	0.045		0.060
Sluggish river reaches, rather weedy or with very deep pools	0.050		0.080
8. Very weedy reaches	0.075		0.150

Adapted from Table 3.1 in Applied Hydrology and Sedimentology for Disturbed Areas

FIGURE 9.3 Riprap Apron Design, Minimum Tailwater Condition



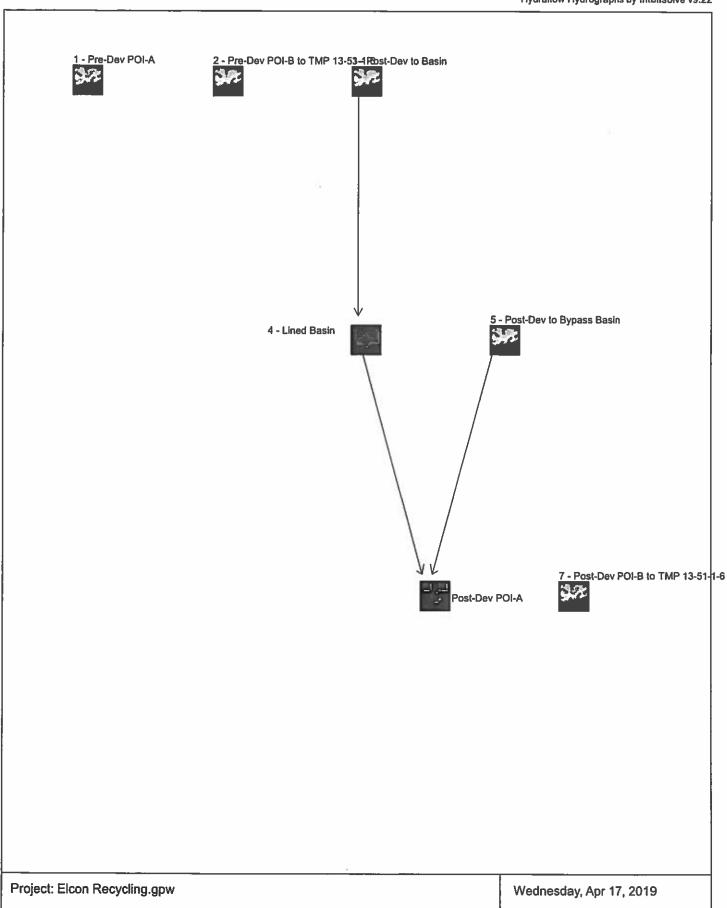
\* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d50 stone size and/or provide velocity reduction device

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PRE-DEVELOPMENT AND POST-DEVELOPMENT HYDROGRAPHS FOR SITE

### **Watershed Model Schematic**

Hydraflow Hydrographs by Intelisolve v9.22



### Hydrograph Return Period Recap

Hydraflow Hydrographs by Intelisolve v9.22

Hyd.	Hydrograph	Hydrograph									
No.	type (origin)	Hyd(s)	1-Yr	2-Yr	3-Үг	5-Yr	flow (cfs) 10-Yr	25-Yr	50-Yr	100-Yr	description
1	SCS Runoff		4.797	8.543	0.008	15.00	21.32	28.06	33.33	40.55	Pre-Dev POI-A
2	SCS Runoff		1.146	2.036	0.002	3.568	5.066	6.657	7.907	9.618	Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff		31.00	39.82	6.800	52.98	64.61	76.16	84.78	96.24	Post-Dev to Basin
4	Reservoir	3	0.301	0.368	0.000	1.148	2.255	3.129	3.663	5.810	Lined Basin
5	SCS Runoff		1.775	2.803	0.010	4.503	6.142	7.846	9.154	10.92	Post-Dev to Bypass Basin
6	Combine	4, 5	2.027	3.092	0.010	4.841	7.283	10.38	12.30	14.75	Post-Dev POI-A
7	SCS Runoff		0.186	0.287	0.000	0.453	0.610	0.777	0.905	1.078	Post-Dev POI-B to TMP 13-51-1-6
										W	
										i	
					e						
				:							
									i		8
l											
Proj	. file: Elcon R	Recycling.	gpw						We	dnesday	, Apr 17, 2019

### **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	4.797	2	730	21,838			******	Pre-Dev POI-A
2	SCS Runoff	1.146	2	728	4,873		******	*****	Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff	31.00	2	718	72,717			*****	Post-Dev to Basin
4	Reservoir	0.301	2	1434	56,698	3	13.98	59,867	Lined Basin
5	SCS Runoff	1.775	2	730	7,138				Post-Dev to Bypass Basin
6	Combine	2.027	2	730	63,836	4, 5			Post-Dev POI-A
7	SCS Runoff	0.186	2	718	377				Post-Dev POI-B to TMP 13-51-1-6
				į					
Elcon Recycling.gpw					Return Period: 1 Year			Wednesday, Apr 17, 2019	

### **Hydrograph Report**

Hydraflow Hydrographs by Intelisotve v9.22

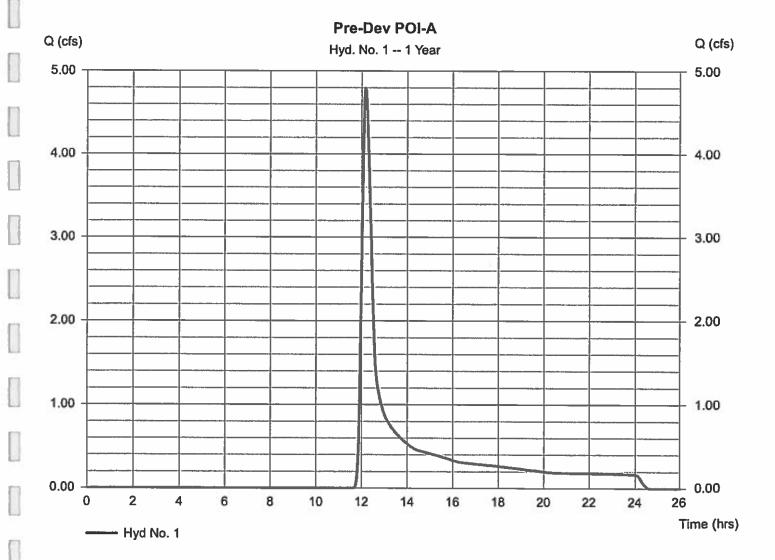
Wednesday, Apr 17, 2019

### Hyd. No. 1

Pre-Dev POI-A

Hydrograph type = SCS Runoff Storm frequency = 1 yrs Time interval = 2 min Drainage area = 11.029 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 2.70 inStorm duration = 24 hrs

Peak discharge = 4.797 cfsTime to peak  $= 12.17 \, hrs$ Hyd. volume = 21,838 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc) = 26.80 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisoive v9.22

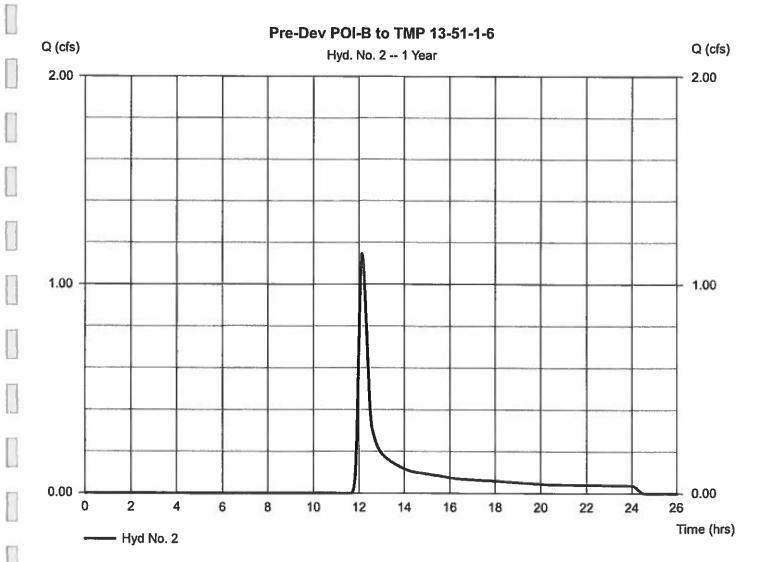
Wednesday, Apr 17, 2019

#### Hyd. No. 2

Pre-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 1 yrs Time interval = 2 min Drainage area = 2.380 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 2.70 inStorm duration = 24 hrs

Peak discharge = 1.146 cfsTime to peak = 12.13 hrsHyd. volume = 4,873 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc) = 23.10 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

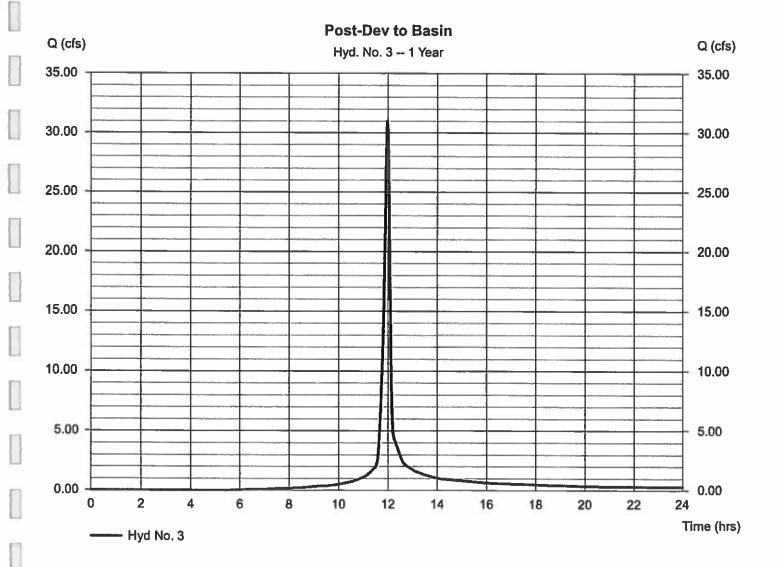
#### Hyd. No. 3

Post-Dev to Basin

Hydrograph type = SCS Runoff Storm frequency = 1 yrs Time interval = 2 min Drainage area = 10.660 ac Basin Slope = 0.0 % Tc method = USER Total precip. = 2.70 inStorm duration = 24 hrs

Peak discharge = 31.00 cfsTime to peak = 11.97 hrs Hyd. volume = 72,717 cuft Curve number = 92 Hydraulic length = 0 ftTime of conc. (Tc) = 8.00 min Distribution = Type II Shape factor

= 484



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 4

Lined Basin

Hydrograph type = Reservoir Storm frequency = 1 yrs Time interval = 2 min

Inflow hyd. No. Reservoir name

= 3 - Post-Dev to Basin

e = Lined Basin

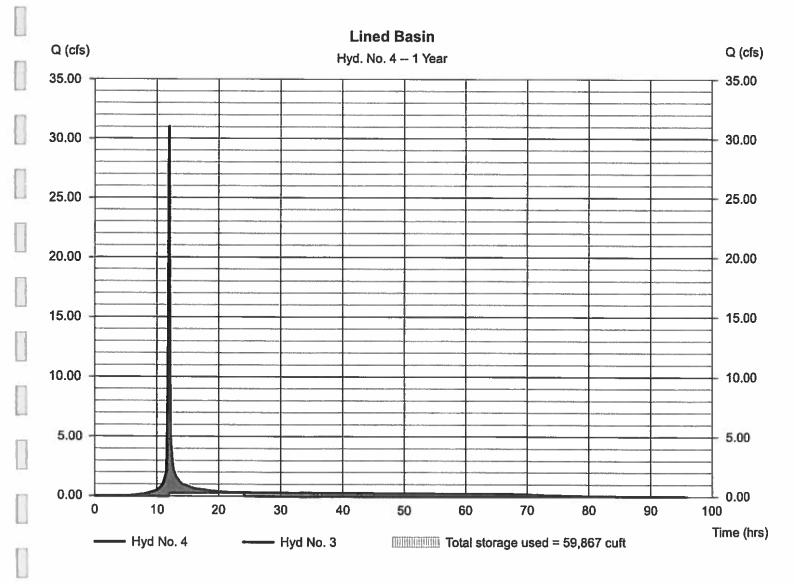
Peak discharge

= 0.301 cfs

Time to peak = 23.90 hrs Hyd. volume = 56,698 cuft Max. Elevation = 13.98 ft

Max. Storage = 59,867 cuft

Storage Indication method used.



## **Pond Report**

Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Pond No. 1 - Lined Basin

#### **Pond Data**

UG Chambers - Invert elev. = 11.25 ft, Rise x Span = 0.33 x 0.33 ft, Barrel Len = 200.00 ft, No. Barrels = 9, Slope = 0.00%, Headers = No Encasement - Invert elev. = 11.25 ft, Width = 20.00 ft, Height = 2.00 ft, Voids = 30.00% Contours - User-defined contour areas. Average end area method used for volume calculation, Begining Elevation = 13.26 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	11.25	n/a	0	0
0.20	11.45	n/a	2,229	2,229
0.40	11.65	n/a	2,200	4,429
0.60	11.85	n/a	2,160	6.589
0.80	12.05	n/a	2,160	8.750
1.00	12.25	n/a	2,160	10.910
1.20	12.45	n/a	2,160	13,070
1.40	12.65	n/a	2,160	15.231
1.60	12.85	n/a	2,160	17,391
1.80	13.05	n/a	2,160	19,552
2.00	13.25	n/a	2,160	21,712
2.01	13.26	51,348	257	21,969
2.75	14.00	53,321	38.728	60,696
3.75	15.00	56,001	54,661	115,357
4.75	16.00	58,738	57,370	172,727
5.75	17.00	61,531	60,135	232,861

#### **Culvert / Orifice Structures**

#### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	6.00	3.25	0.00	Crest Len (ft)	= 12.00	90.00	0.00	0.00
Span (in)	= 15.00	18.00	3.25	0.00	Crest El. (ft)	= 15.60	16.30	0.00	0.00
No. Barrels	= 1	1	1	0	Weir Coeff.	= 3.33	2.60	3.33	3,33
Invert El. (ft)	= 12.50	14.35	12.67	0.00	Weir Type	= Rect	Broad		_
Length (ft)	= 66.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 0.50	0.00	0.00	n/a	•				
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (b)	(Contour)		
Multi-Stage	= n/a	Yes	Yes	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Welr risers checked for orifice conditions (ic) and submergence (s).

#### Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	CIv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfii cfs	User cfs	Total cfs
0.00	0	11.25	0.00	0.00	0.00	-	0.00	0.00		_	_	_	0.000
0.20	2,229	11.45	0.00	0.00	0.00	***	0.00	0.00	_	***			0.000
0.40	4,429	11.65	0.00	0.00	0.00	_	0.00	0.00			_	_	0.000
0.60	6,589	11.85	0.00	0.00	0.00		0.00	0.00	_	_			0.000
0.80	8,750	12.05	0.00	0.00	0.00	_	0.00	0.00			_	_	0.000
1.00	10,910	12.25	0.00	0.00	0.00		0.00	0.00	_				0.000
1.20	13,070	12.45	0.00	0.00	0.00		0.00	0.00					0.000
1.40	15,231	12.65	0.00	0.00	0.00		0.00	0.00	_	_			0.000
1.60	17,391	12.85	0.06 ic	0.00	0.06 ic		0.00	0.00	•••		_		0.059
1.80	19,552	13.05	0.14 ic	0.00	0.14 lc	***	0.00	0.00	_	_			0.137
2.00	21,712	13,25	0,18 ic	0.00	0.18 ic	_	0.00	0.00			_	_	0.185
2.01	21,969	13.26	0.19 ic	0.00	0.19 ic		0.00	0.00		_	_		0.187
2.75	60,696	14.00	0.31 ic	0.00	0.30 ic		0.00	0.00	_				0.303
3.75	115,357	15.00	2.65 oc	2.28 ic	0.35 ic	-	0.00	0.00			_	_	2.636
4.75	172,727	16.00	8.87 oc	1.31 ic	0.10 lc		7.45 s	0.00		_			8.864
5.75	232,861	17.00	10.71 oc	0.31 lc	0.02 ic	_	10.32 s	137.05			_	_	147.71

Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 5

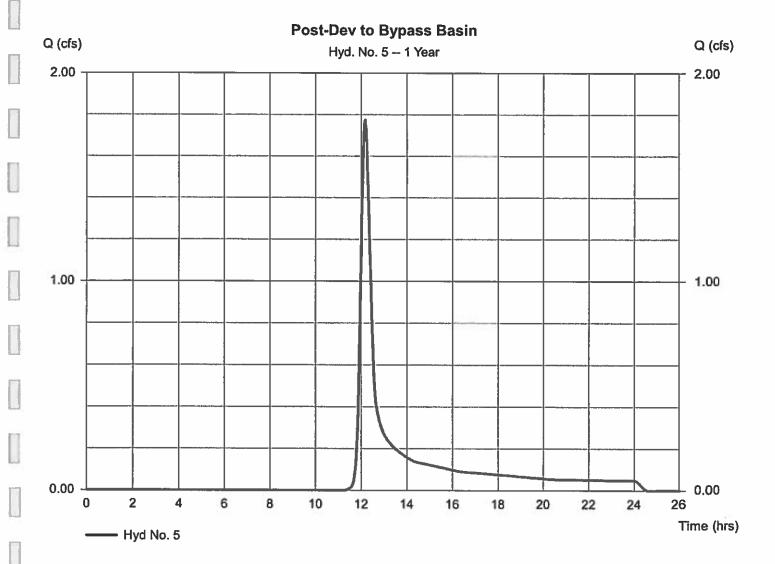
#### Post-Dev to Bypass Basin

Hydrograph type = SCS Runoff Storm frequency = 1 yrsTime interval = 2 min Drainage area = 2.593 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 2.70 inStorm duration = 24 hrs

Peak discharge = 1.775 cfs
Time to peak = 12.17 hrs
Hyd. volume = 7,138 cuft
Curve number = 75
Hydraulic length = 0 ft
Time of conc. (Tc) = 23.77 min
Distribution = Type II

= 484

Shape factor



Hydraflow Hydrographs by Intelisolve v9.22

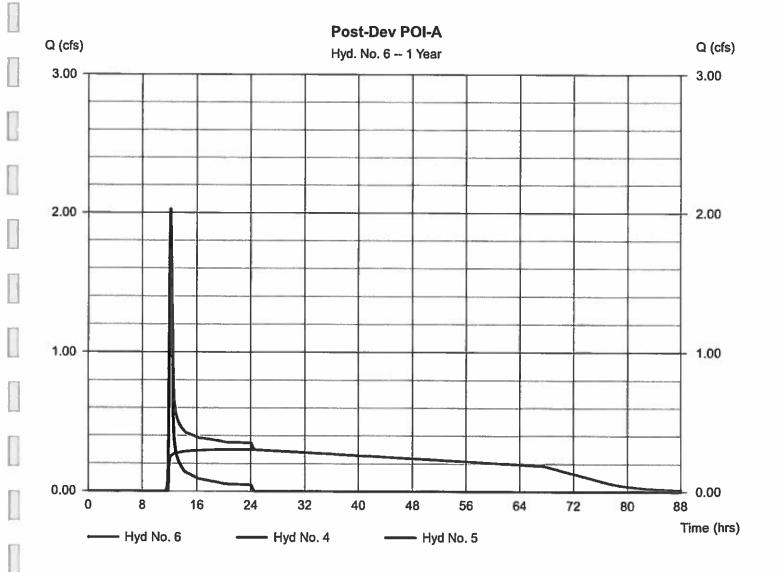
Wednesday, Apr 17, 2019

### Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine
Storm frequency = 1 yrs
Time interval = 2 min
Inflow hyds. = 4, 5

Peak discharge = 2.027 cfs
Time to peak = 12.17 hrs
Hyd. volume = 63,836 cuft
Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisoive v9.22

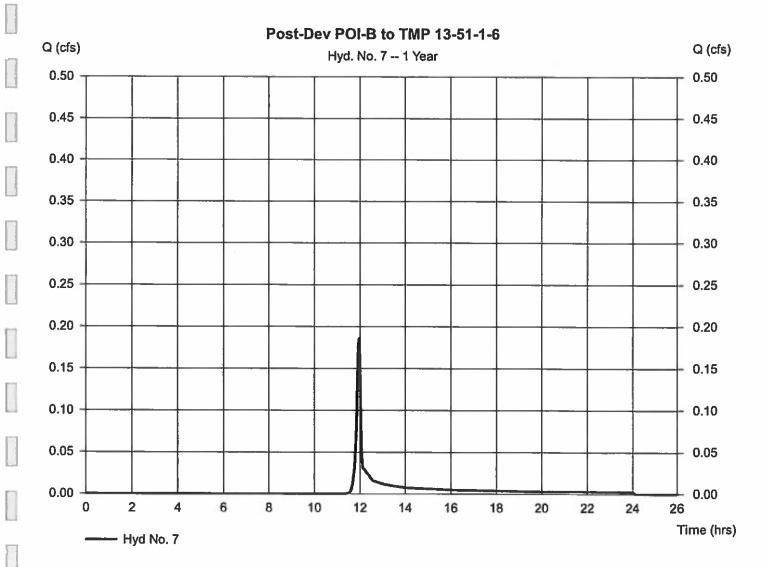
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 1 yrs Time interval = 2 min Drainage area = 0.153 acBasin Slope = 0.0 %Tc method = USER Total precip. = 2.70 inStorm duration = 24 hrs

Peak discharge = 0.186 cfsTime to peak  $= 11.97 \, hrs$ Hyd. volume = 377 cuft Curve number = 74 Hydraulic length = 0 ftTime of conc. (Tc)  $= 5.00 \, \text{min}$ = Type II Distribution Shape factor = 484



# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	8.543	2	730	34,952	_			Pre-Dev POI-A
2	SCS Runoff	2.036	2	728	7,799				Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff	39.82	2	718	94,641				Post-Dev to Basin
4	Reservoir	0.368	2	1440	77,565	3	14.34	79,450	Lined Basin
5	SCS Runoff	2.803	2	730	10,768	****		—	Post-Dev to Bypass Basin
6	Combine	3.092	2	730	88,334	4,5			Post-Dev POI-A
7	SCS Runoff	0.287	2	718	575	_			Post-Dev POI-B to TMP 13-51-1-6
	- Decree				-				
⊏ICO	n Recycling.g	jpw 			Return P	eriod: 2 Ye	ar 	Wednesday	y, Apr 17, 2019

Hydraflow Hydrographs by Intelisolve v9.22

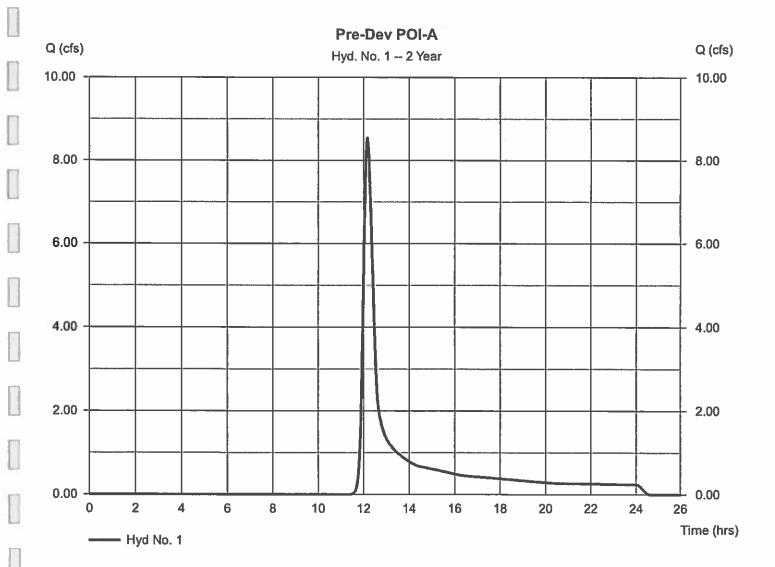
Wednesday, Apr 17, 2019

#### Hyd. No. 1

Pre-Dev POI-A

Hydrograph type = SCS Runoff Storm frequency = 2 yrs = 2 min Time interval Drainage area = 11.029 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 3.30 inStorm duration = 24 hrs

Peak discharge = 8.543 cfsTime to peak = 12.17 hrsHyd. volume = 34,952 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc)  $= 26.80 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

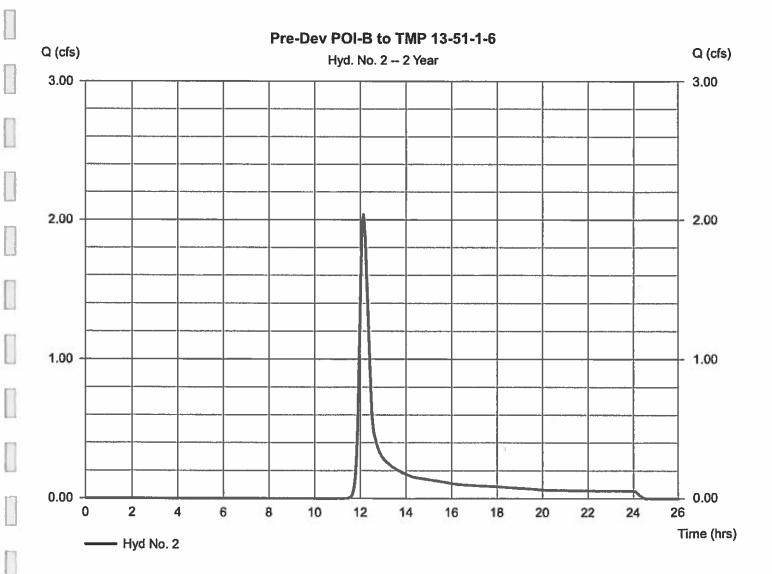
Wednesday, Apr 17, 2019

#### Hyd. No. 2

Pre-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 2 yrs Time interval = 2 min Drainage area = 2.380 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 3.30 inStorm duration = 24 hrs

Peak discharge = 2.036 cfsTime to peak = 12.13 hrs Hyd. volume = 7,799 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc)  $= 23.10 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisotve v9.22

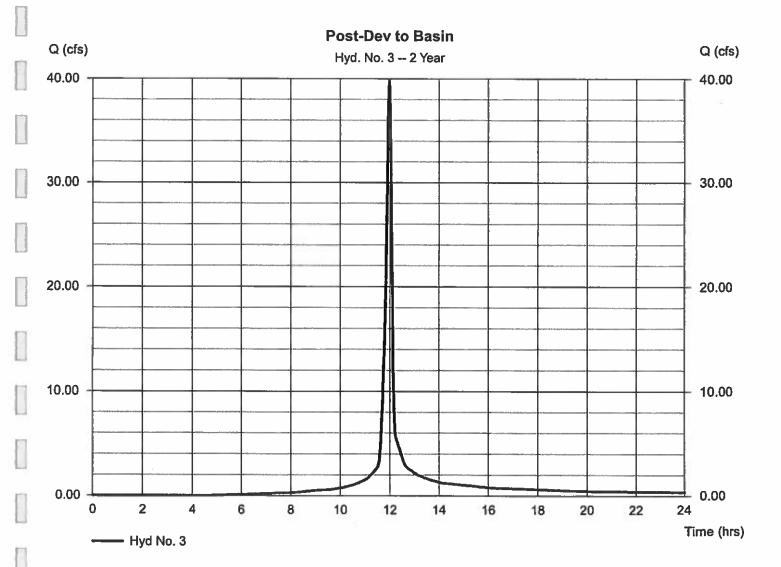
Wednesday, Apr 17, 2019

#### Hyd. No. 3

#### Post-Dev to Basin

Hydrograph type = SCS Runoff Storm frequency = 2 yrs = 2 min Time interval Drainage area = 10.660 ac Basin Slope = 0.0 %Tc method = USER Total precip. = 3.30 inStorm duration = 24 hrs

Peak discharge = 39.82 cfsTime to peak = 11.97 hrs Hyd. volume = 94,641 cuft Curve number = 92 Hydraulic length = 0 ftTime of conc. (Tc) = 8.00 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

### Hyd. No. 4

**Lined Basin** 

Hydrograph type = Reservoir Storm frequency = 2 yrs Time interval = 2 min

Inflow hyd. No. Reservoir name

= 3 - Post-Dev to Basin

= Lined Basin

Peak discharge

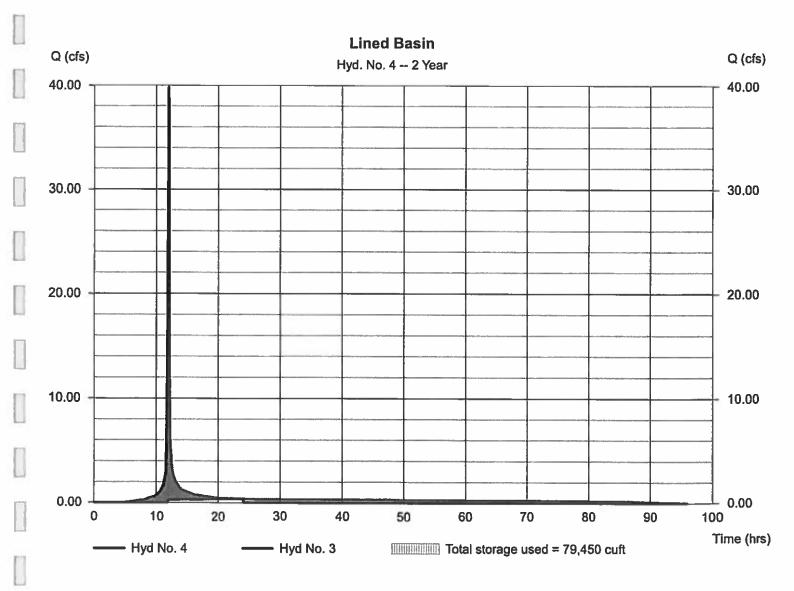
= 0.368 cfs

Time to peak Hyd. volume

= 24.00 hrs = 77,565 cuft

Max. Elevation Max. Storage = 14.34 ft = 79,450 cuft

Storage Indication method used.



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

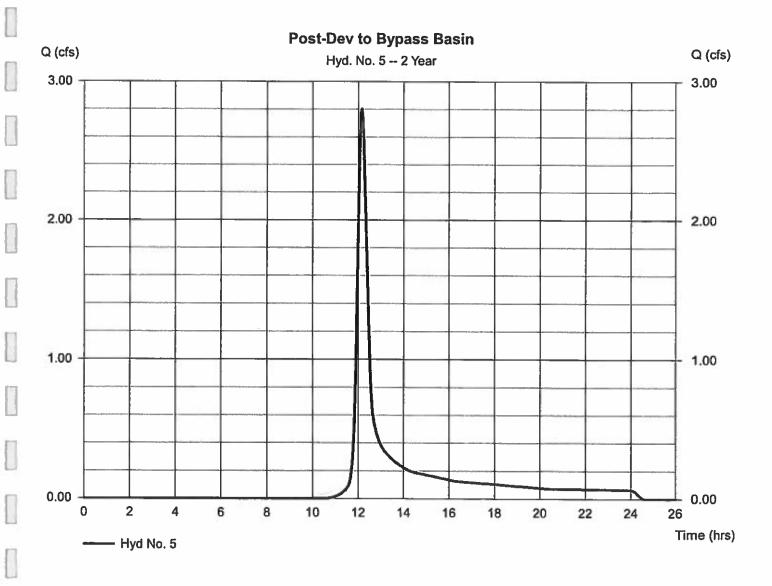
### Hyd. No. 5

Post-Dev to Bypass Basin

Hydrograph type = SCS Runoff Storm frequency = 2 yrs = 2 min Time interval Drainage area = 2.593 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 3.30 inStorm duration = 24 hrs

Peak discharge = 2.803 cfs
Time to peak = 12.17 hrs
Hyd. volume = 10,768 cuft
Curve number = 75

Hydraulic length = 0 ft
Time of conc. (Tc) = 23.77 min
Distribution = Type II
Shape factor = 484



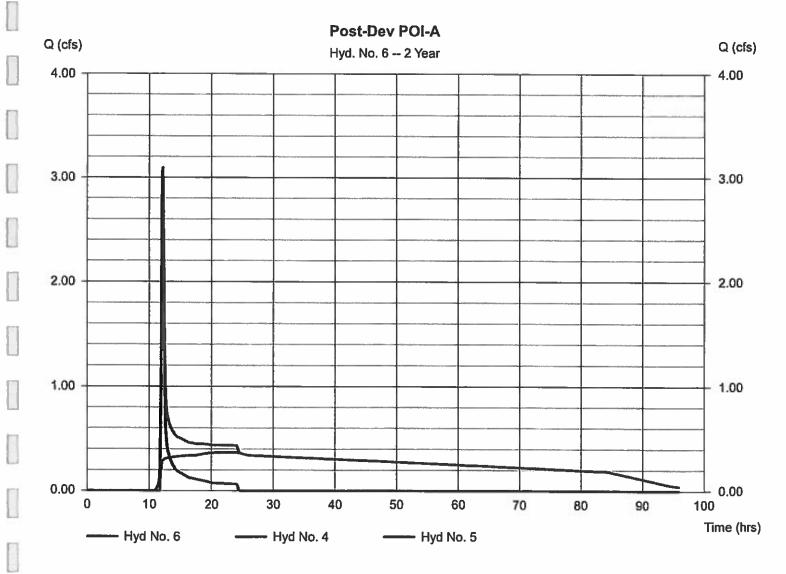
Hydraflow Hydrographs by Intelisoive v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 2 min Inflow hyds. = 4, 5 Peak discharge = 3.092 cfs
Time to peak = 12.17 hrs
Hyd. volume = 88,334 cuft
Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisotve v9.22

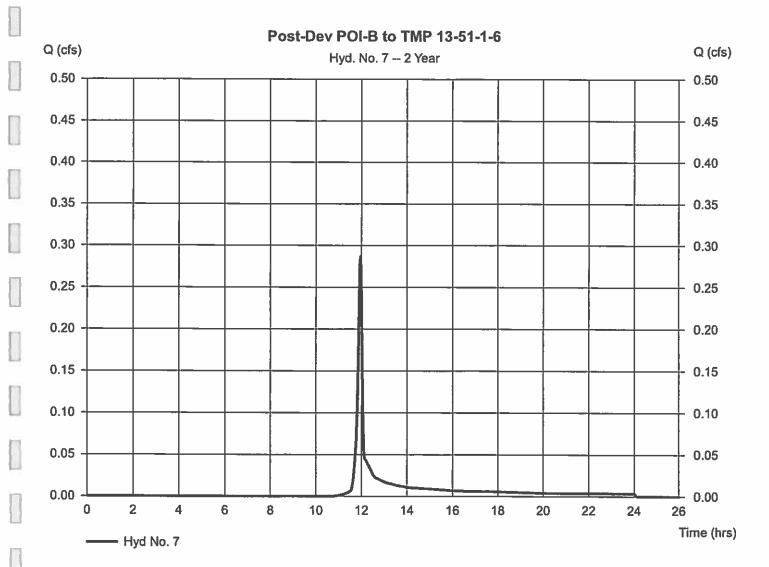
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 2 yrs Time interval = 2 min Drainage area = 0.153 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.30 inStorm duration = 24 hrs

Peak discharge = 0.287 cfsTime to peak = 11.97 hrsHyd. volume = 575 cuft Curve number = 74 Hydraulic length = 0 ftTime of conc. (Tc)  $= 5.00 \, \text{min}$ Distribution = Type II Shape factor = 484



# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.22

2 3 4 1 5 5 6 0	SCS Runoff SCS Runoff SCS Runoff Reservoir SCS Runoff Combine SCS Runoff	0.008 0.002 6.800 0.000 0.010	2 2 2	1440 1440	182 41	_			Pre-Dev POI-A
3   4   1   5   6   6	SCS Runoff Reservoir SCS Runoff Combine	6.800 0.000	2		41	1		į.	FIE-DEV POI-A
5 5 6 0	Reservoir SCS Runoff Combine	0.000			1 77	_			Pre-Dev POI-B to TMP 13-51-1-6
5 6	SCS Runoff	1	_	720	15,573		—		Post-Dev to Basin
6	Combine	0.010	2	n/a	0	3	12.68	15,573	Lined Basin
1 1		1	2	790	281		<u> </u>	<u> </u>	Post-Dev to Bypass Basin
7 3	SCS Runoff	0.010	2	790	281	4, 5			Post-Dev POI-A
		0.000	2	806	12	–	<u></u>		Post-Dev POI-B to TMP 13-51-1-6
Elcor									

Hydraflow Hydrographs by Intelisolve v9.22

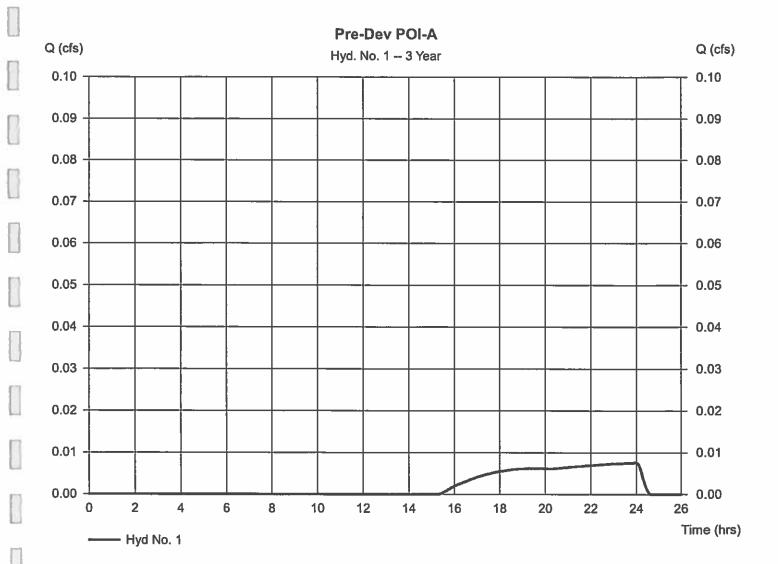
Wednesday, Apr 17, 2019

#### Hyd. No. 1

Pre-Dev POI-A

Hydrograph type = SCS Runoff Storm frequency = 3 yrsTime interval = 2 min Drainage area = 11.029 ac Basin Slope = 0.0 % Tc method = TR55 Total precip. = 1.00 inStorm duration = 24 hrs

Peak discharge = 0.008 cfsTime to peak  $= 24.00 \, hrs$ Hyd. volume = 182 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc) = 26.80 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisoive v9.22

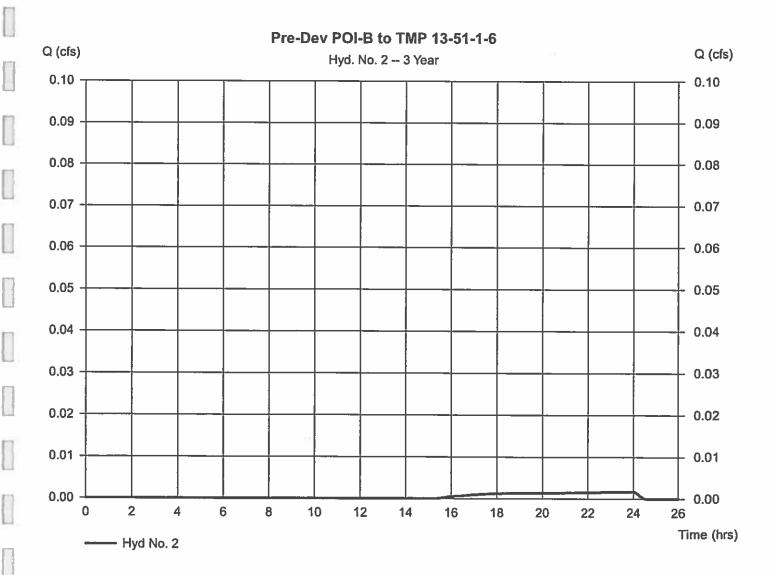
Wednesday, Apr 17, 2019

#### Hyd. No. 2

Pre-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 3 yrs Time interval = 2 min Drainage area = 2.380 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 1.00 inStorm duration = 24 hrs

Peak discharge = 0.002 cfsTime to peak  $= 24.00 \, hrs$ Hyd. volume = 41 cuft Curve number = 70 Hydraulic length = 0 ft= 23.10 min Time of conc. (Tc) Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

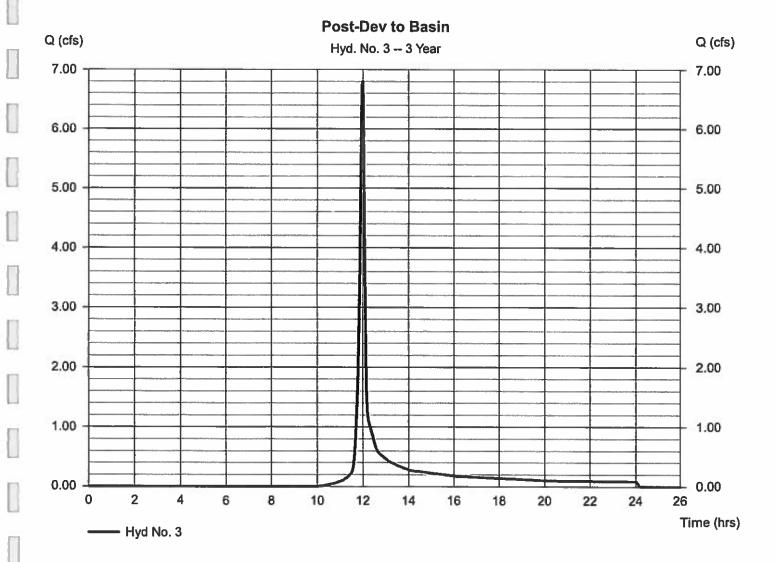
Wednesday, Apr 17, 2019

### Hyd. No. 3

Post-Dev to Basin

Hydrograph type = SCS Runoff Storm frequency = 3 yrsTime interval = 2 minDrainage area = 10.660 acBasin Slope = 0.0 % Tc method = USER Total precip. = 1.00 inStorm duration = 24 hrs

= 6.800 cfsPeak discharge Time to peak = 12.00 hrsHyd. volume = 15,573 cuft Curve number = 92 Hydraulic length = 0 ftTime of conc. (Tc) = 8.00 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisoive v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 4

Lined Basin

Hydrograph type = Reservoir Storm frequency = 3 yrsTime interval = 2 min

Inflow hyd. No. = 3 - Post-Dev to Basin Reservoir name

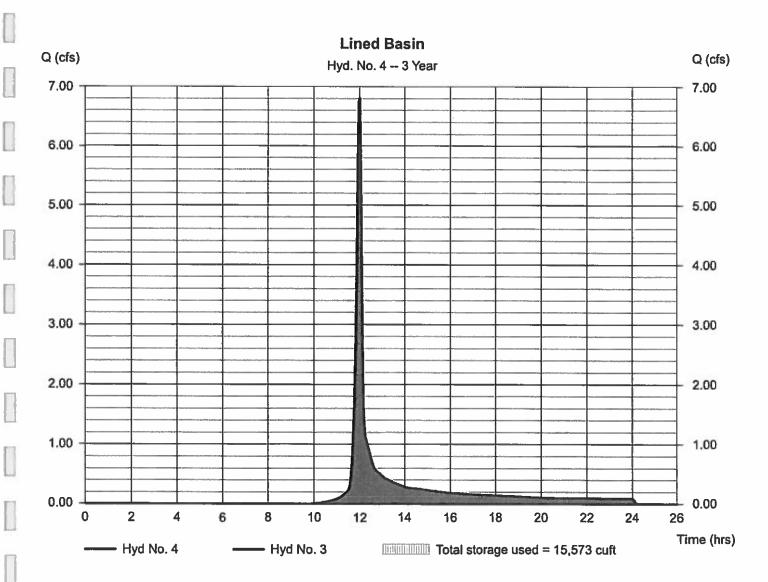
= Lined Basin

Peak discharge = 0.000 cfs

Time to peak = n/aHyd. volume = 0 cuft

Max. Elevation = 12.68 ftMax. Storage = 15,573 cuft

Storage Indication method used.



Hydraflow Hydrographs by Intelisoive v9.22

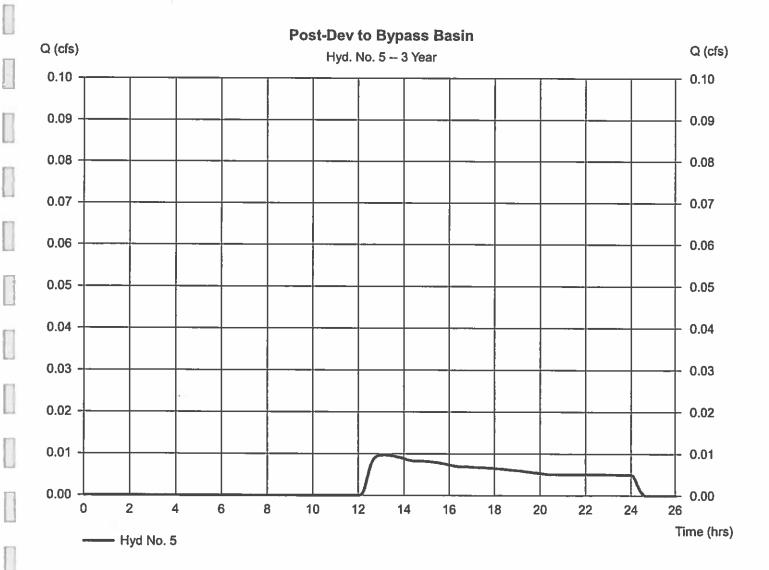
Wednesday, Apr 17, 2019

#### Hyd. No. 5

Post-Dev to Bypass Basin

Hydrograph type = SCS Runoff Storm frequency = 3 yrs= 2 min Time interval Drainage area = 2.593 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 1.00 inStorm duration = 24 hrs

Peak discharge = 0.010 cfsTime to peak = 13.17 hrs Hyd. volume = 281 cuft Curve number = 75 Hydraulic length = 0 ftTime of conc. (Tc)  $= 23.77 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

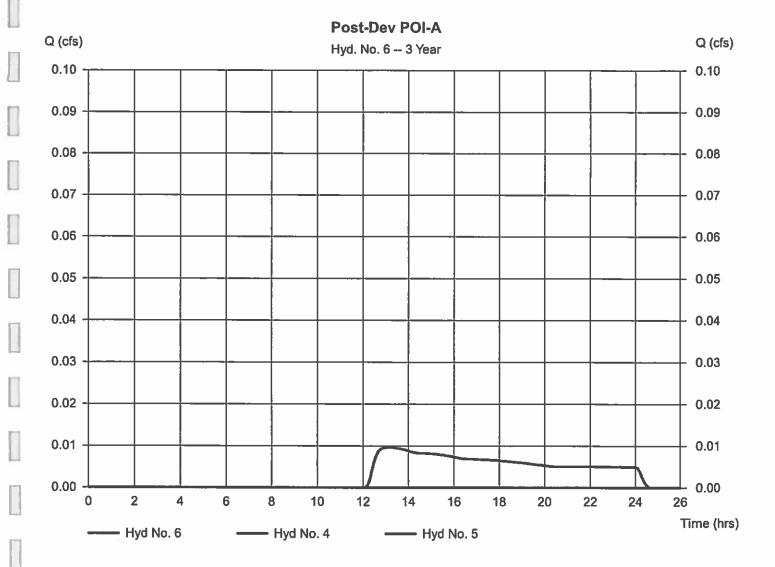
Wednesday, Apr 17, 2019

### Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine
Storm frequency = 3 yrs
Time interval = 2 min
Inflow hyds. = 4, 5

Peak discharge = 0.010 cfs
Time to peak = 13.17 hrs
Hyd. volume = 281 cuft
Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisolve v9.22

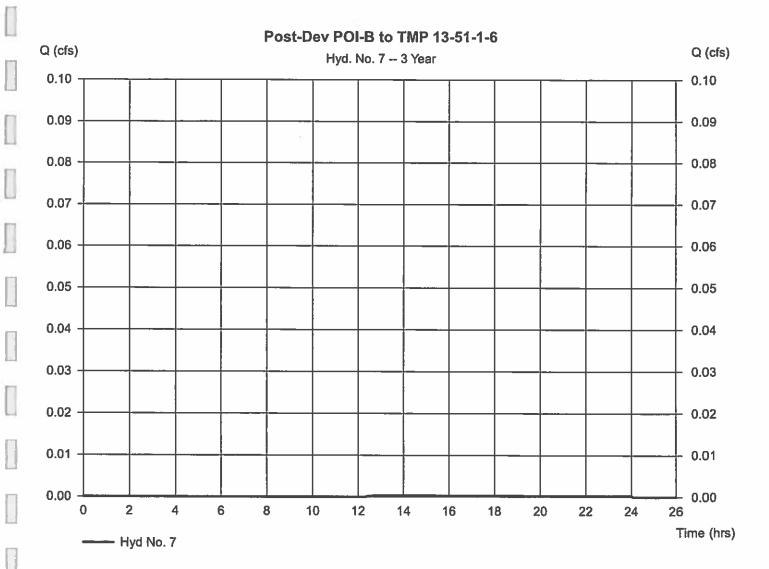
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 3 yrsTime interval = 2 min Drainage area = 0.153 acBasin Slope = 0.0 % Tc method = USER Total precip. = 1.00 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak  $= 13.43 \, hrs$ Hyd. volume = 12 cuft Curve number = 74 Hydraulic length = 0 ftTime of conc. (Tc)  $= 5.00 \, \text{min}$ Distribution = Type II Shape factor = 484



# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time Interval (min)	Time to peak (min)	Hyd. volume (cuft)	inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	15.00	2	730	57,729	****		9-9-1-1-1	Pre-Dev POI-A
2	SCS Runoff	3.568	2	728	12,881	****			Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff	52.98	2	718	128,121	****	direction and the second		Post-Dev to Basin
4	Reservoir	1.148	2	936	109,686	3	14.64	95,519	Lined Basin
5	SCS Runoff	4.503	2	730	16,846				Post-Dev to Bypass Basin
6	Combine	4.841	2	730	126,532	4, 5			Post-Dev POI-A
7	SCS Runoff	0.453	2	718	908				Post-Dev POI-B to TMP 13-51-1-6
#5									
	,								
Elco	on Recycling.	gpw			Return P	eriod: 5 Ye	ar	Wednesda	l y, Apr 17, 2019

Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

### Hyd. No. 1

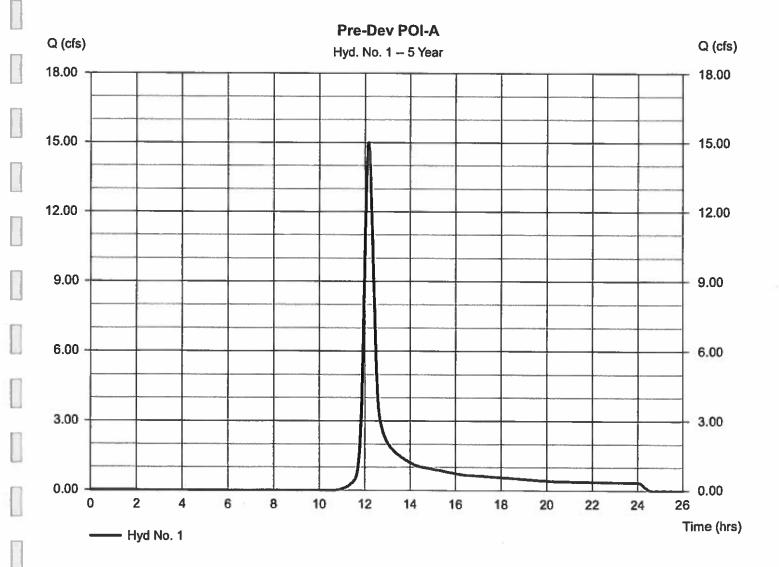
Pre-Dev POI-A

Hydrograph type = SCS Runoff Storm frequency = 5 yrsTime interval = 2 min Drainage area = 11.029 ac Basin Slope = 0.0 % Tc method = TR55 Total precip. = 4.20 inStorm duration = 24 hrs

Peak discharge = 15.00 cfs
Time to peak = 12.17 hrs
Hyd. volume = 57,729 cuft
Curve number = 70
Hydraulic length = 0 ft
Time of conc. (Tc) = 26.80 min
Distribution = Type II

= 484

Shape factor



Hydraflow Hydrographs by Intelisoive v9.22

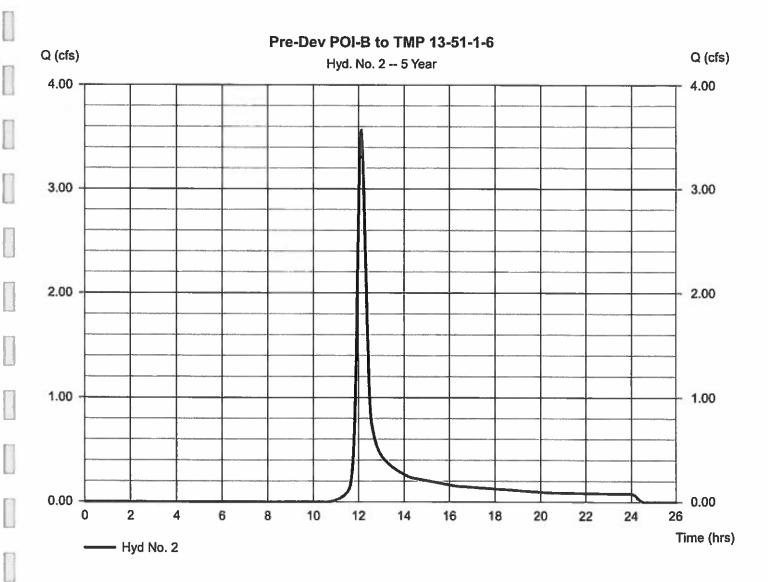
Wednesday, Apr 17, 2019

#### Hyd. No. 2

Pre-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 5 yrs Time interval = 2 min Drainage area = 2.380 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 4.20 inStorm duration = 24 hrs

Peak discharge = 3.568 cfsTime to peak = 12.13 hrsHyd. volume = 12,881 cuft= 70 Curve number Hydraulic length = 0 ftTime of conc. (Tc) = 23.10 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 3

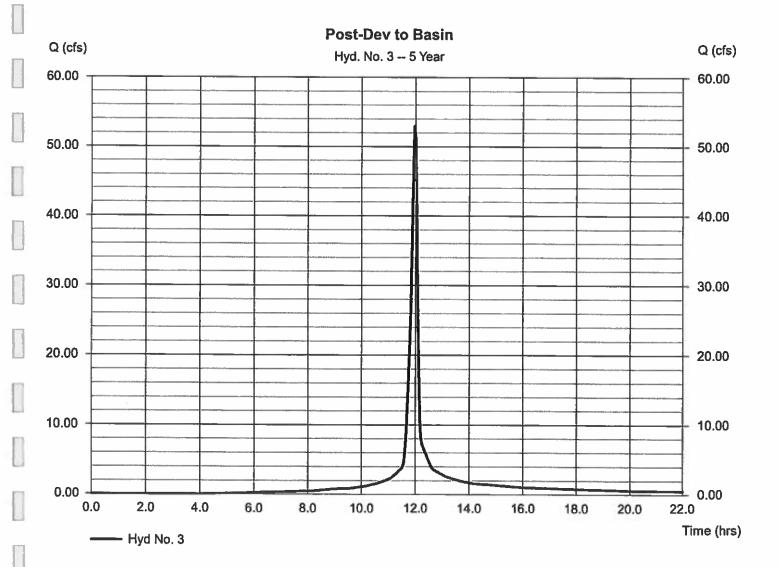
Post-Dev to Basin

Hydrograph type = SCS Runoff Storm frequency = 5 yrsTime interval = 2 min Drainage area = 10.660 ac Basin Slope = 0.0 %Tc method = USER Total precip. = 4.20 inStorm duration = 24 hrs

Peak discharge = 52.98 cfs
Time to peak = 11.97 hrs
Hyd. volume = 128,121 cuft
Curve number = 92
Hydraulic length = 0 ft
Time of conc. (Tc) = 8.00 min
Distribution = Type II

= 484

Shape factor



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 4

**Lined Basin** 

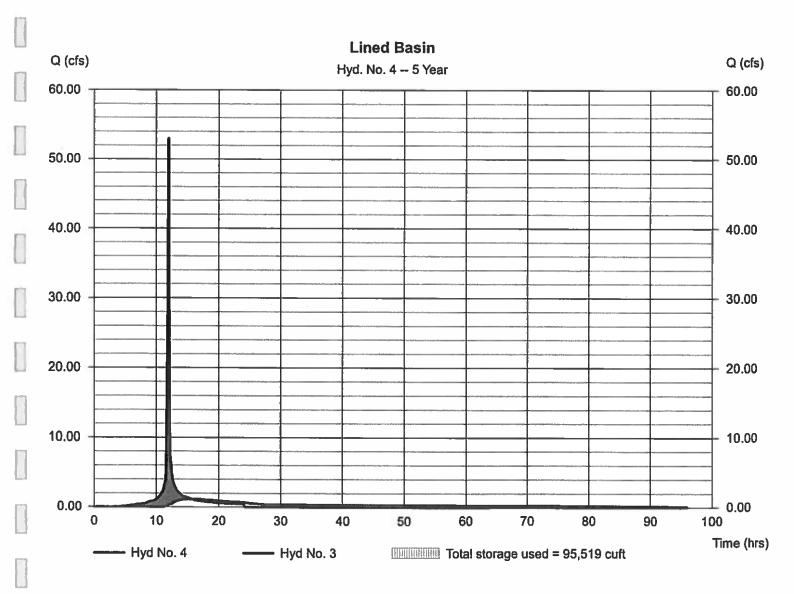
Hydrograph type = Reservoir Storm frequency = 5 yrs Time interval = 2 min

Inflow hyd. No. = 3 - Post-Dev to Basin Reservoir name = Lined Basin Peak discharge = 1. Time to peak = 15

= 1.148 cfs = 15.60 hrs

Hyd. volume = 109,686 cuft
Max. Elevation = 14.64 ft
Max. Storage = 95,519 cuft

Storage Indication method used.



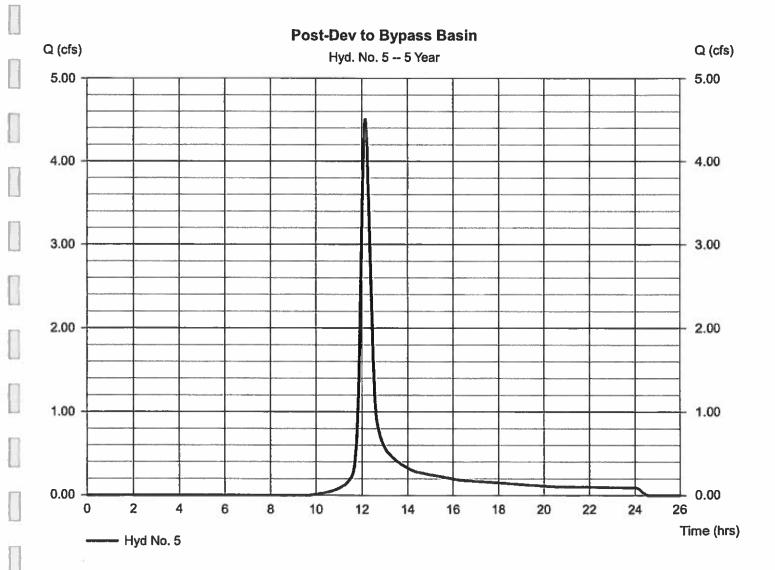
Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

### Hyd. No. 5

Post-Dev to Bypass Basin

Hydrograph type = SCS Runoff Peak discharge = 4.503 cfsStorm frequency = 5 yrs Time to peak  $= 12.17 \, hrs$ = 2 min Time interval Hyd. volume = 16,846 cuft Drainage area = 2.593 ac Curve number = 75 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc)  $= 23.77 \, \text{min}$ Total precip. = 4.20 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



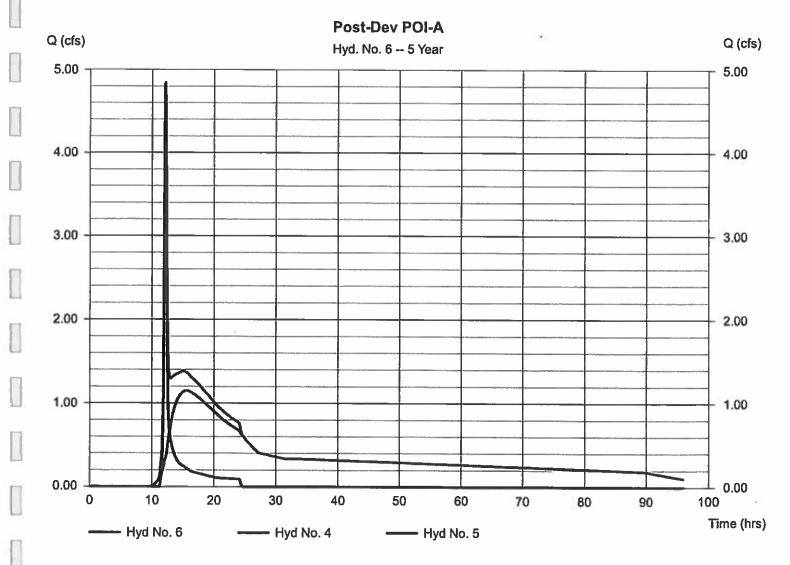
Hydraflow Hydrographs by Intelisoive v9.22

Wednesday, Apr 17, 2019

### Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine Storm frequency = 5 yrs Time interval = 2 min Inflow hyds. = 4, 5 Peak discharge = 4.841 cfs Time to peak = 12.17 hrs Hyd. volume = 126,532 cuft Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisolve v9.22

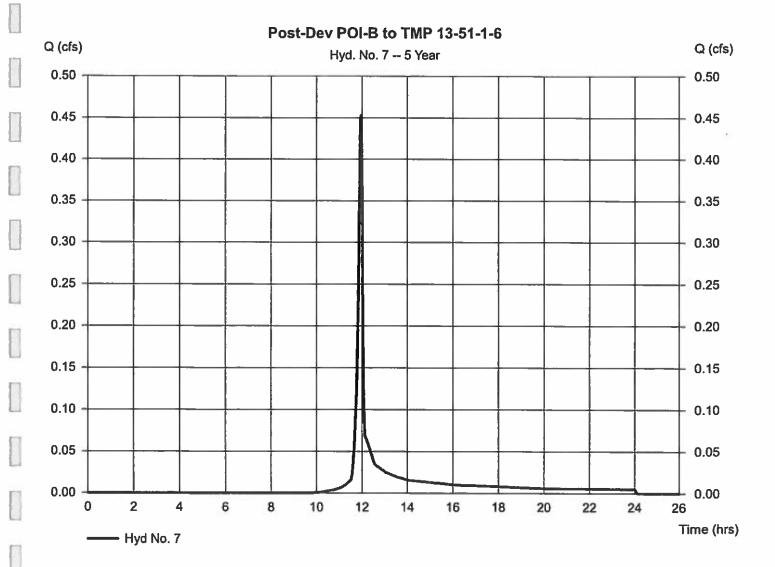
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 5 yrs Time interval = 2 min Drainage area = 0.153 acBasin Slope = 0.0 % Tc method = USER Total precip. = 4.20 inStorm duration = 24 hrs

Peak discharge = 0.453 cfsTime to peak  $= 11.97 \, hrs$ Hyd. volume = 908 cuft Curve number = 74 Hydraulic length = 0 ftTime of conc. (Tc)  $= 5.00 \, \text{min}$ Distribution = Type II Shape factor = 484



# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time Interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	21.32	2	730	80,251			******	Pre-Dev POI-A
2	SCS Runoff	5.066	2	728	17,907	****		V-00000	Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff	64.61	2	718	158,238	****		*****	Post-Dev to Basin
4	Reservoir	2.255	2	828	139,405	3	14.88	108,966	Lined Basin
5	SCS Runoff	6.142	2	728	22,694				Post-Dev to Bypass Basin
6	Combine	7.283	2	730	162,098	4, 5			Post-Dev POI-A
7	SCS Runoff	0.610	2	716	1,231	****			Post-Dev POI-B to TMP 13-51-1-6
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	n Recycling.	L			Return D	eriod: 10 Y	ear	Wednesday	<u> </u> y, Apr 17, 2019

Hydraflow Hydrographs by Intelisolve v9.22

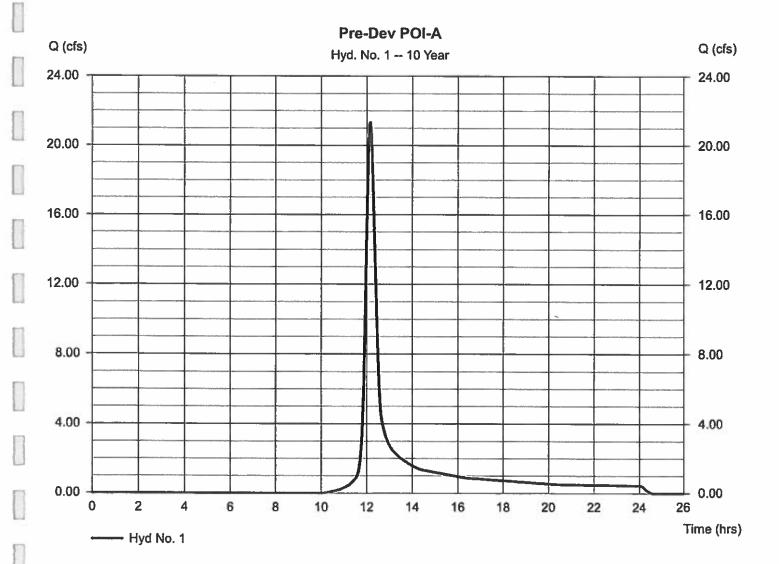
Wednesday, Apr 17, 2019

#### Hyd. No. 1

Pre-Dev POI-A

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 minDrainage area = 11.029 ac Basin Slope = 0.0 % Tc method = TR55 Total precip. = 5.00 inStorm duration = 24 hrs

Peak discharge = 21.32 cfsTime to peak  $= 12.17 \, hrs$ Hyd. volume = 80,251 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc) = 26.80 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

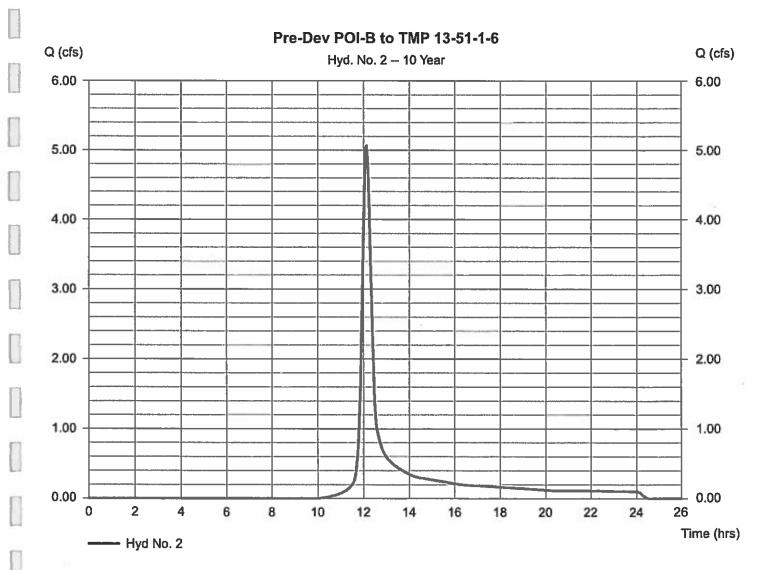
Wednesday, Apr 17, 2019

#### Hyd. No. 2

Pre-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 10 yrs Time interval = 2 min Drainage area = 2.380 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 5.00 inStorm duration = 24 hrs

Peak discharge = 5.066 cfsTime to peak  $= 12.13 \, hrs$ Hyd. volume = 17,907 cuft Curve number = 70Hydraulic length = 0 ftTime of conc. (Tc)  $= 23.10 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisoive v9.22

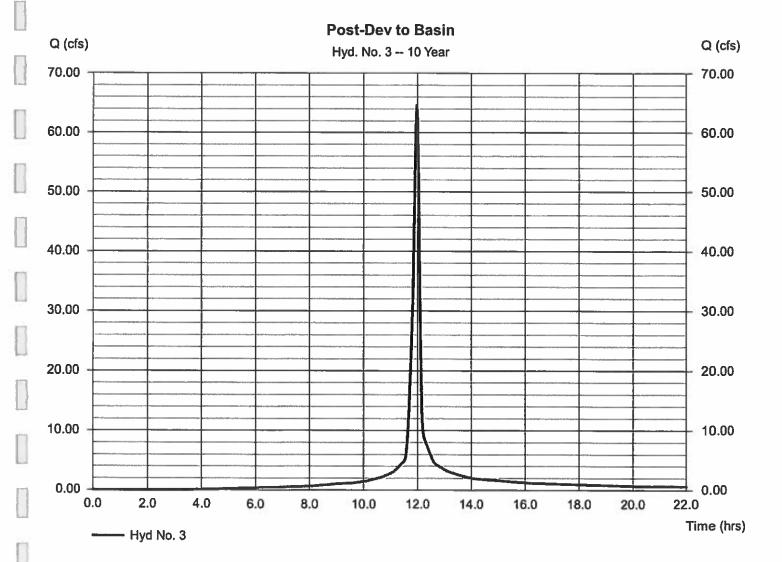
Wednesday, Apr 17, 2019

#### Hyd. No. 3

Post-Dev to Basin

Hydrograph type = SCS Runoff Storm frequency = 10 yrs Time interval = 2 min Drainage area = 10.660 ac Basin Slope = 0.0 % Tc method = USER Total precip. = 5.00 inStorm duration = 24 hrs

Peak discharge = 64.61 cfsTime to peak = 11.97 hrs Hyd. volume = 158,238 cuft Curve number = 92 Hydraulic length = 0 ftTime of conc. (Tc)  $= 8.00 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 4

Lined Basin

Hydrograph type = Reservoir Storm frequency = 10 yrs Time interval = 2 min

Inflow hyd. No. Reservoir name

= 3 - Post-Dev to Basin

= Lined Basin

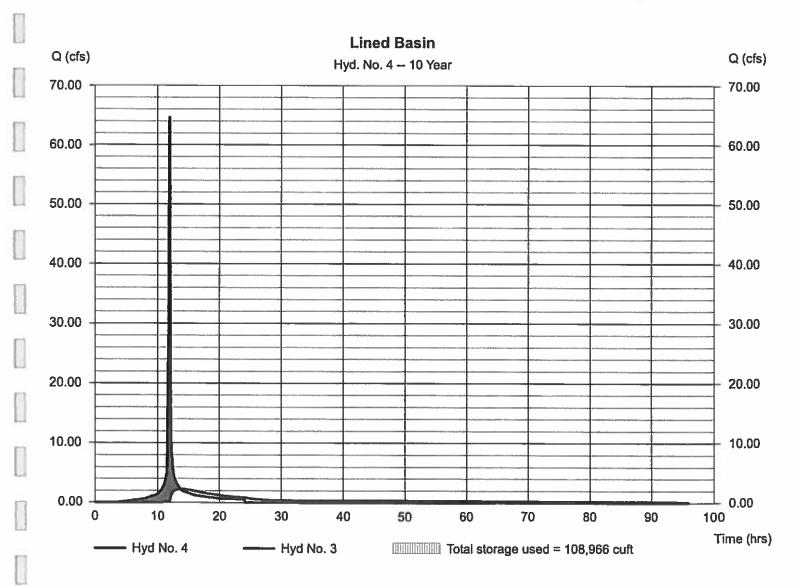
Peak discharge Time to peak

= 2.255 cfs = 13.80 hrs

Hyd. volume = 139,405 cuft Max. Elevation = 14.88 ft

Max. Storage = 108,966 cuft

Storage Indication method used.



Hydraflow Hydrographs by Intelisoive v9.22

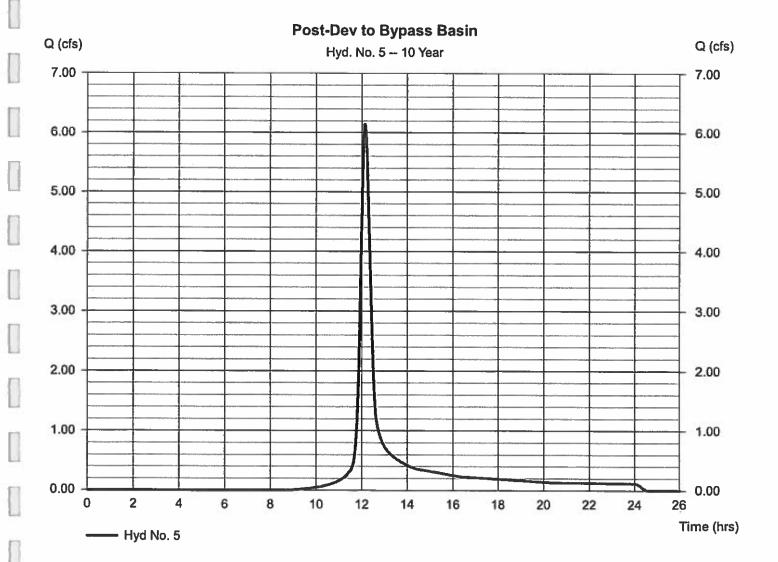
Wednesday, Apr 17, 2019

#### Hyd. No. 5

Post-Dev to Bypass Basin

Hydrograph type = SCS Runoff Storm frequency = 10 yrs Time interval = 2 min Drainage area = 2.593 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 5.00 inStorm duration = 24 hrs

Peak discharge = 6.142 cfsTime to peak  $= 12.13 \, hrs$ Hyd. volume = 22,694 cuft Curve number = 75 Hydraulic length = 0 ftTime of conc. (Tc)  $= 23.77 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

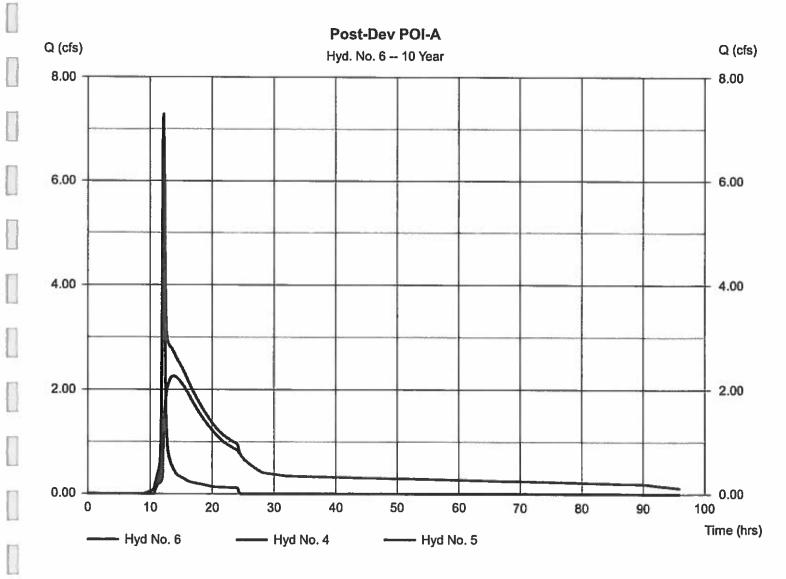
Wednesday, Apr 17, 2019

#### Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyds. = 4, 5

Peak discharge = 7.283 cfs Time to peak = 12.17 hrs Hyd. volume = 162,098 cuft Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisolve v9.22

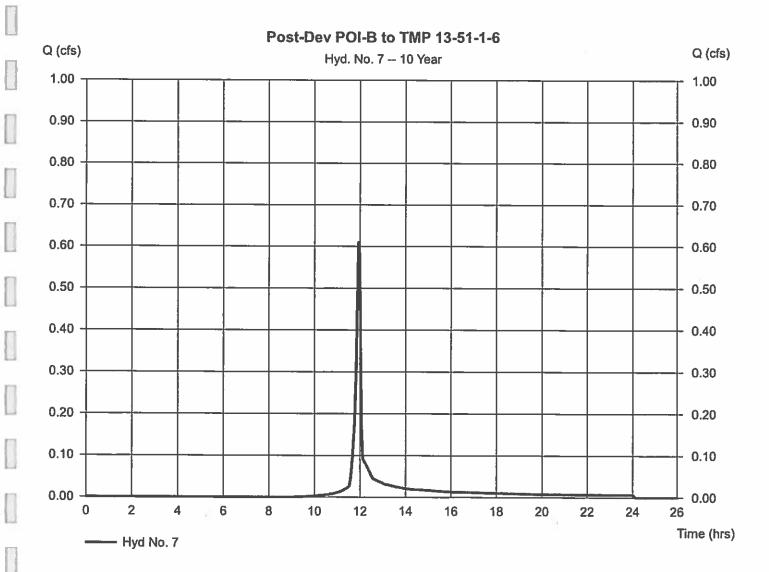
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min Drainage area = 0.153 acBasin Slope = 0.0 % Tc method = USER Total precip. = 5.00 inStorm duration = 24 hrs

Peak discharge = 0.610 cfsTime to peak = 11.93 hrsHyd. volume = 1,231 cuft Curve number = 74 Hydraulic length = 0 ftTime of conc. (Tc) = 5.00 min Distribution = Type II Shape factor = 484



# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time Interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	28.06	2	728	104,334		*****		Pre-Dev POI-A
2	SCS Runoff	6.657	2	726	23,280		******		Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff	76.16	2	718	188,562		******		Post-Dev to Basin
4	Reservoir	3.129	2	806	169,369	3	15.19	126,303	Lined Basin
5	SCS Runoff	7.846	2	728	28,837	<del></del>		<del></del>	Post-Dev to Bypass Basin
6	Combine	10.38	2	730	198,206	4, 5			Post-Dev POI-A
7	SCS Runoff	0.777	2	716	1,571		******		Post-Dev POI-B to TMP 13-51-1-6
Elco	n Recycling.	jpw			Return P	eriod: 25 Y	ear	Wednesday	y, Apr 17, 2019

Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 1

Pre-Dev POI-A

Hydrograph type = SCS Runoff Storm frequency = 25 yrs Time interval = 2 min Drainage area = 11.029 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 5.80 inStorm duration = 24 hrs

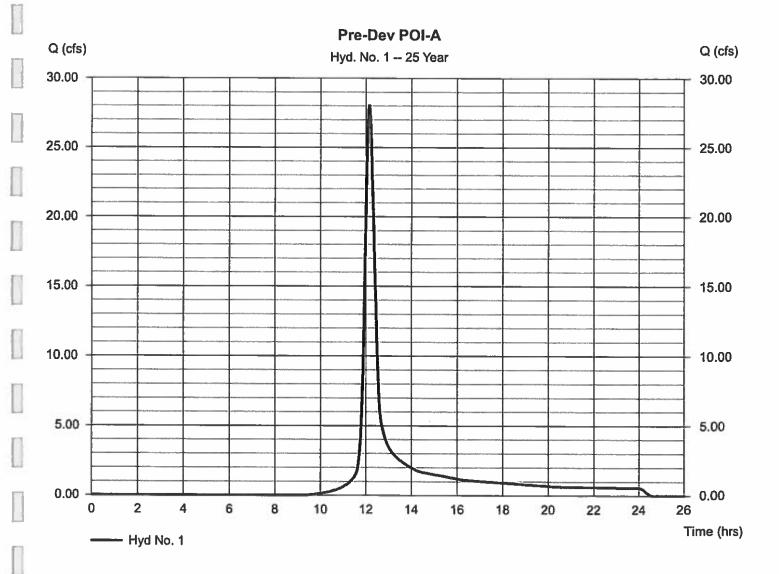
Peak discharge = 28.06 cfs
Time to peak = 12.13 hrs
Hyd. volume = 104,334 cuft
Curve number = 70
Hydraulic length = 0 ft
Time of conc. (Tc) = 26.80 min

= Type II

= 484

Distribution

Shape factor



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 2

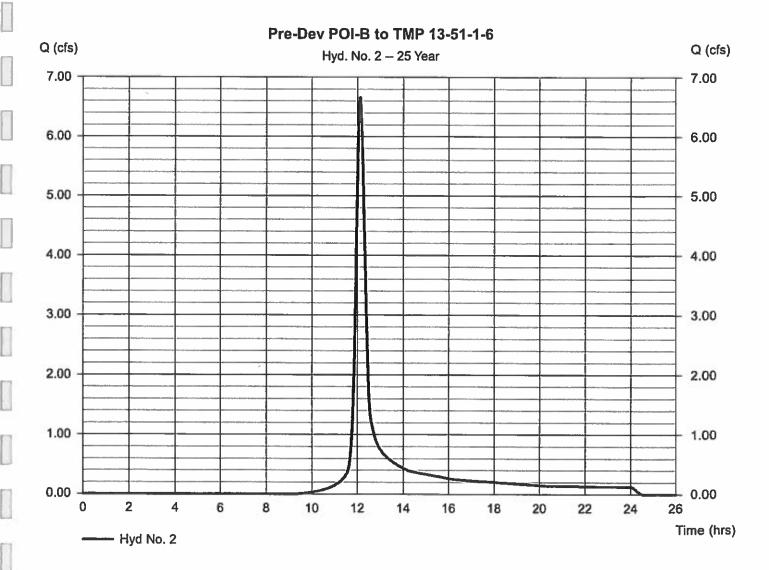
Pre-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 25 yrs Time interval = 2 min Drainage area = 2.380 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 5.80 inStorm duration = 24 hrs

Peak discharge = 6.657 cfs
Time to peak = 12.10 hrs
Hyd. volume = 23,280 cuft
Curve number = 70
Hydraulic length = 0 ft
Time of conc. (Tc) = 23.10 min
Distribution = Type II

= 484

Shape factor



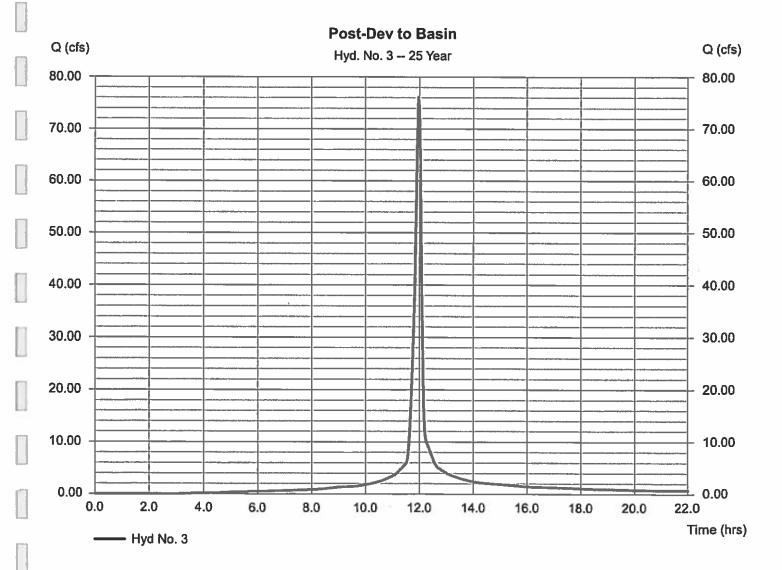
Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 3

Post-Dev to Basin

= SCS Runoff Hydrograph type Peak discharge = 76.16 cfs Storm frequency = 25 yrsTime to peak = 11.97 hrs = 2 min Time interval Hyd. volume = 188,562 cuft Drainage area = 10.660 ac Curve number = 92 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = USER Time of conc. (Tc)  $= 8.00 \, \text{min}$ Total precip. = 5.80 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 4

Lined Basin

Hydrograph type = Reservoir Storm frequency = 25 yrs Time interval = 2 min

Inflow hyd. No. = 3 - Post-Dev to Basin Reservoir name

= Lined Basin

Peak discharge

= 3.129 cfs $= 13.43 \, hrs$ 

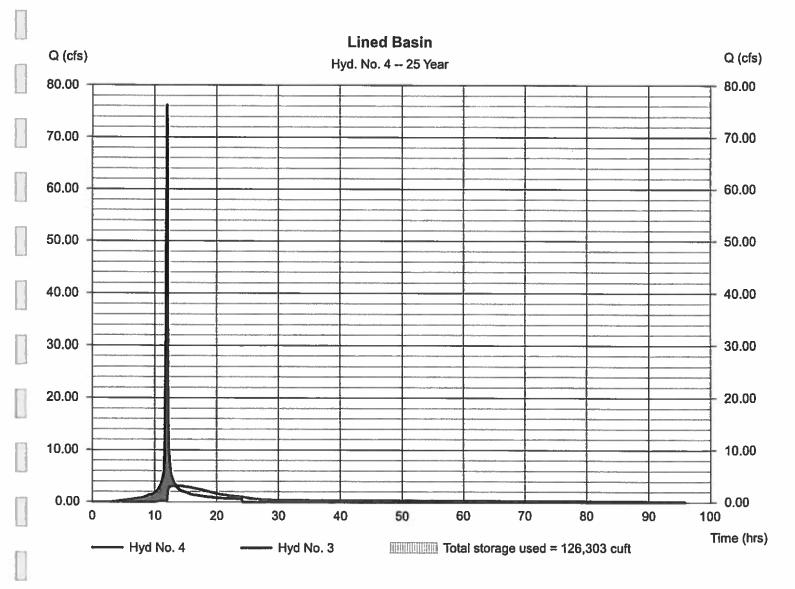
Time to peak Hyd. volume

= 169,369 cuft

Max. Elevation  $= 15.19 \, \mathrm{ft}$ 

Max. Storage = 126,303 cuft

Storage Indication method used.



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

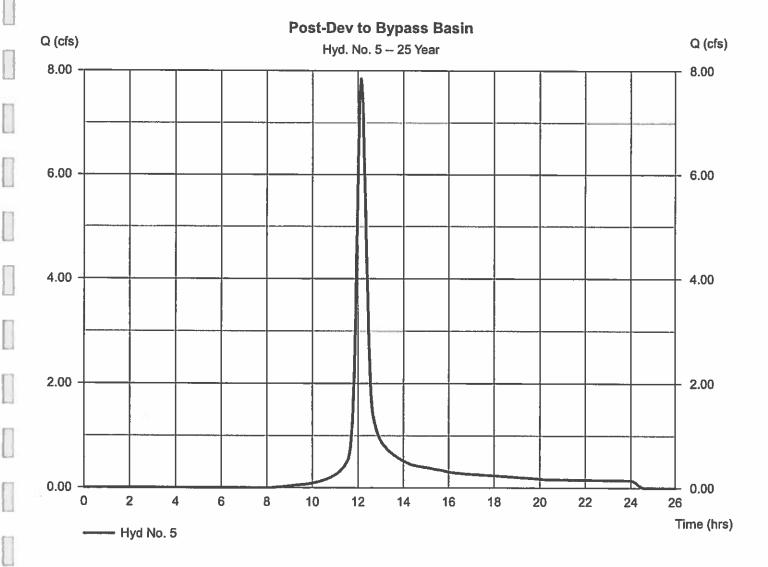
#### Hyd. No. 5

Post-Dev to Bypass Basin

= SCS Runoff Hydrograph type Storm frequency = 25 yrs = 2 min Time interval Drainage area = 2.593 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 5.80 inStorm duration = 24 hrs

Peak discharge = 7.846 cfs
Time to peak = 12.13 hrs
Hyd. volume = 28,837 cuft
Curve number = 75

Hydraulic length = 0 ft
Time of conc. (Tc) = 23.77 min
Distribution = Type II
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

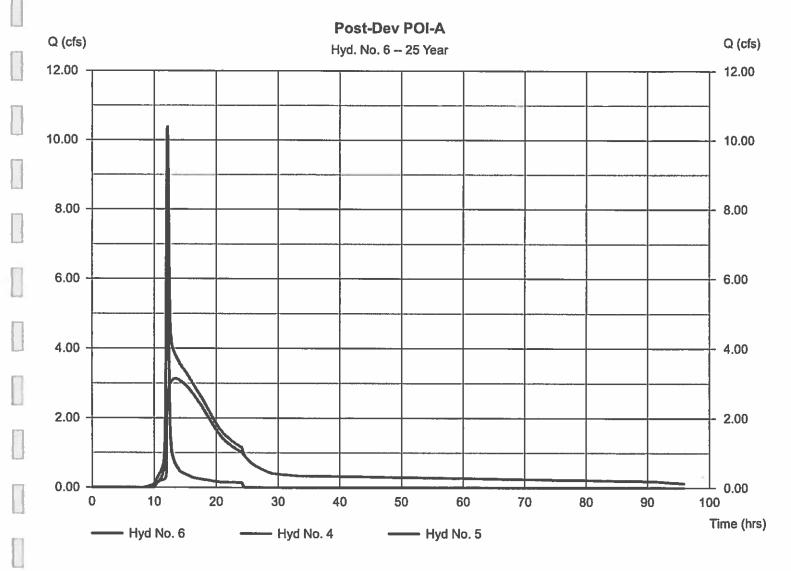
Wednesday, Apr 17, 2019

#### Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine Storm frequency = 25 yrs Time interval = 2 min Inflow hyds. = 4, 5

Peak discharge = 10.38 cfs
Time to peak = 12.17 hrs
Hyd. volume = 198,206 cuft
Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisolve v9.22

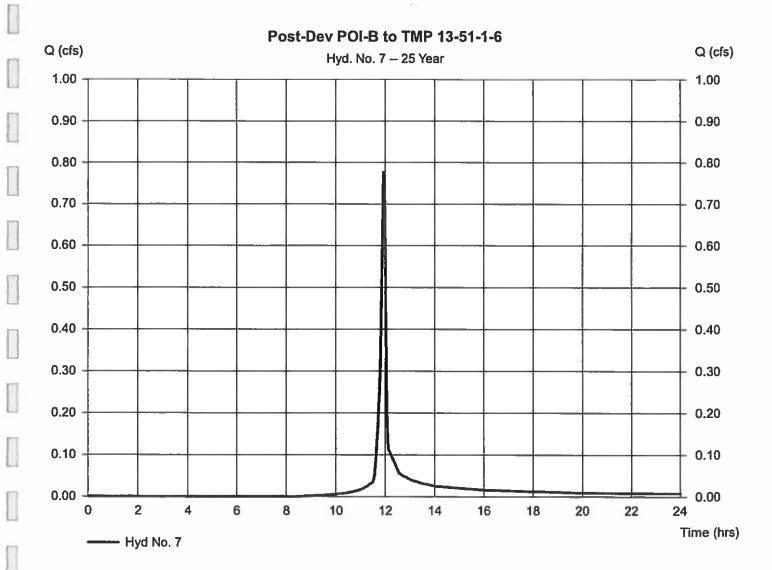
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 25 yrs Time interval = 2 min Drainage area = 0.153 acBasin Slope = 0.0 % = USER Tc method Total precip. = 5.80 inStorm duration = 24 hrs

Peak discharge = 0.777 cfsTime to peak  $= 11.93 \, hrs$ Hyd. volume = 1,571 cuftCurve number = 74 Hydraulic length = 0 ftTime of conc. (Tc)  $= 5.00 \, \text{min}$ Distribution = Type II Shape factor = 484



# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisoive v9.22

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	33.33	2	728	123,191	_	******	****	Pre-Dev POI-A
2	SCS Runoff	7.907	2	726	27,488		******	****	Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff	84.78	2	718	211,398		*******		Post-Dev to Basin
4	Reservoir	3.663	2	800	191,911	3	15.44	140,696	Lined Basin
5	SCS Runoff	9.154	2	728	33,592			*****	Post-Dev to Bypass Basin
6	Combine	12.30	2	730	225,503	4, 5	******		Post-Dev POI-A
7	SCS Runoff	0.905	2	716	1,835		*******		Post-Dev POI-B to TMP 13-51-1-6
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	on Recycling.	now.		*>	Poture P	eriod: 50 Y	'aar	Modpoodo	y, Apr 17, 2019

Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

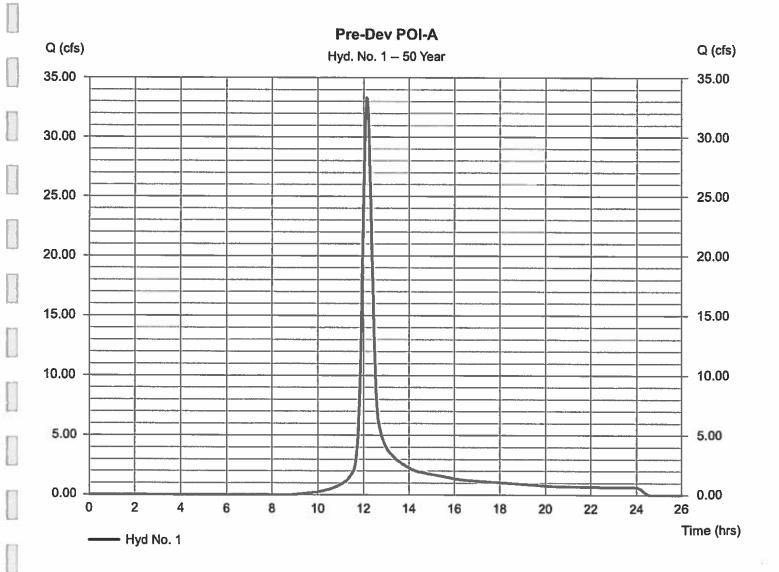
#### Hyd. No. 1

Pre-Dev POI-A

Hydrograph type = SCS Runoff Storm frequency = 50 yrsTime interval = 2 min Drainage area = 11.029 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 33.33 cfs
Time to peak = 12.13 hrs
Hyd. volume = 123,191 cuft
Curve number = 70
Hydraulic length = 0 ft
Time of conc. (Tc) = 26.80 min

Time of conc. (Tc) = 26.80 min
Distribution = Type !!
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

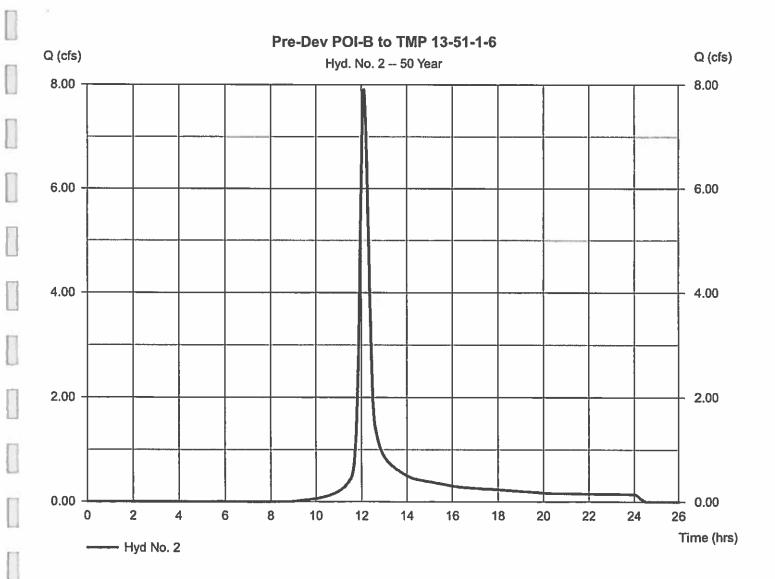
Wednesday, Apr 17, 2019

#### Hyd. No. 2

Pre-Dev POI-B to TMP 13-51-1-6

= SCS Runoff Hydrograph type = 50 yrs Storm frequency Time interval = 2 min Drainage area = 2.380 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 7.907 cfsTime to peak  $= 12.10 \, hrs$ Hyd. volume = 27,488 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc) = 23.10 min Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

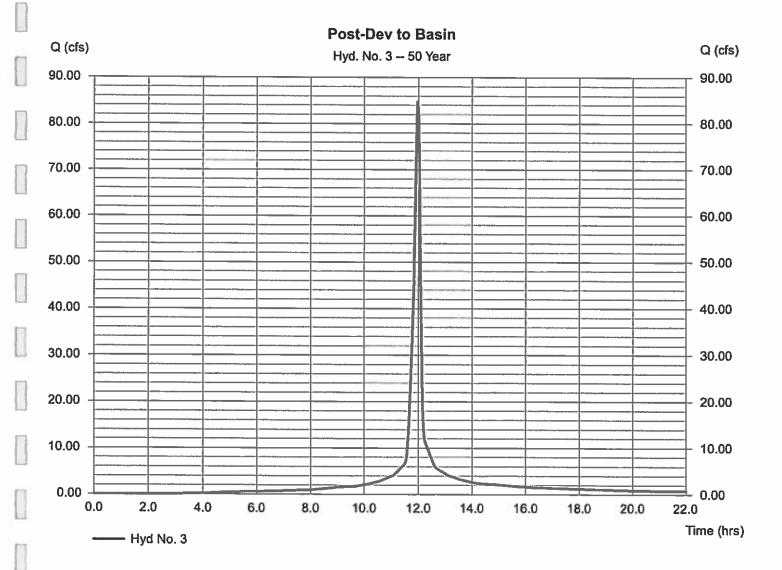
Wednesday, Apr 17, 2019

#### Hyd. No. 3

Post-Dev to Basin

Hydrograph type = SCS Runoff Storm frequency = 50 yrs Time interval = 2 min Drainage area = 10.660 ac Basin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 84.78 cfsTime to peak  $= 11.97 \, hrs$ Hyd. volume = 211,398 cuft Curve number = 92 Hydraulic length = 0 ftTime of conc. (Tc)  $= 8.00 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 4

Lined Basin

Hydrograph type = Reservoir Storm frequency = 50 yrs Time interval = 2 min

Inflow hyd. No. Reservoir name = 3 - Post-Dev to Basin

= Lined Basin

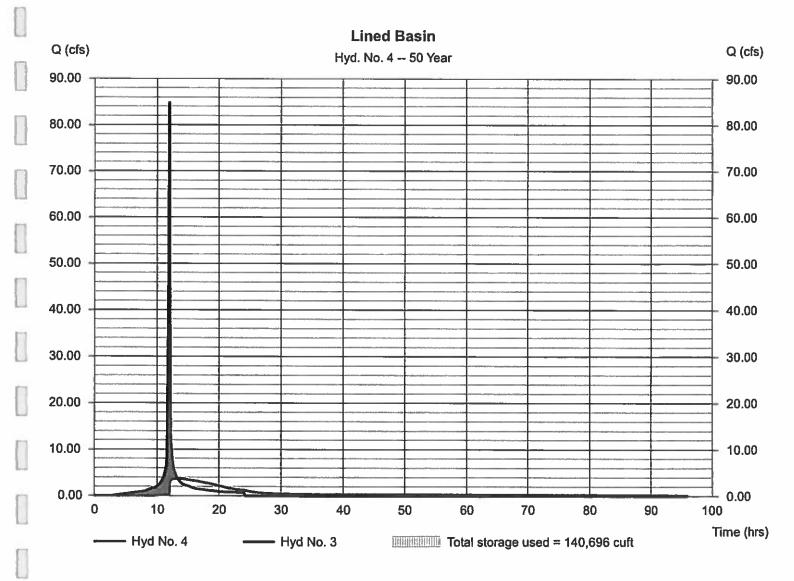
Peak discharge

= 3.663 cfs

Time to peak  $= 13.33 \, hrs$ Hyd. volume = 191,911 cuft Max. Elevation  $= 15.44 \, \mathrm{ft}$ 

Max. Storage = 140,696 cuft

Storage Indication method used.



Hydraflow Hydrographs by Intelisoive v9.22

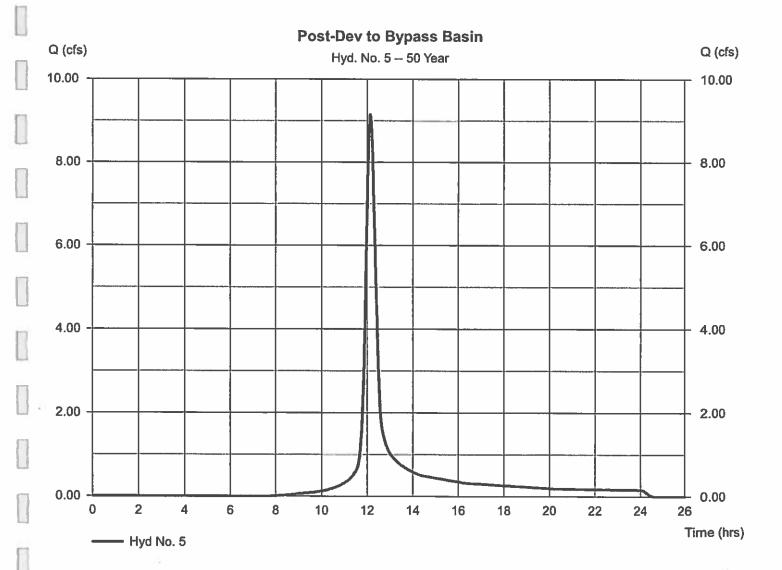
Wednesday, Apr 17, 2019

#### Hyd. No. 5

Post-Dev to Bypass Basin

Hydrograph type = SCS Runoff Storm frequency = 50 yrsTime interval  $= 2 \min$ Drainage area = 2.593 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 9.154 cfsTime to peak = 12.13 hrs Hyd. volume = 33,592 cuft Curve number = 75 Hydraulic length = 0 ftTime of conc. (Tc) = 23.77 min Distribution = Type II Shape factor = 484



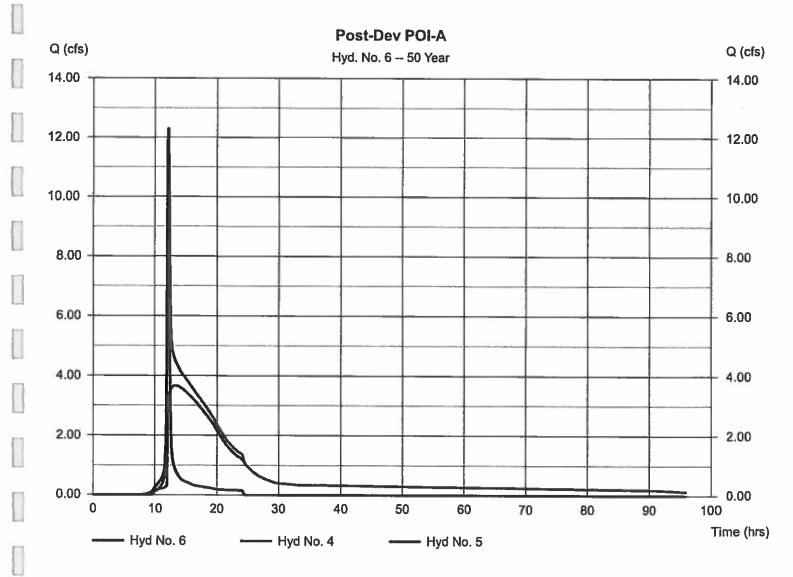
Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine Storm frequency = 50 yrs Time interval = 2 min Inflow hyds. = 4, 5 Peak discharge = 12.30 cfs Time to peak = 12.17 hrs Hyd. volume = 225,503 cuft Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisolve v9.22

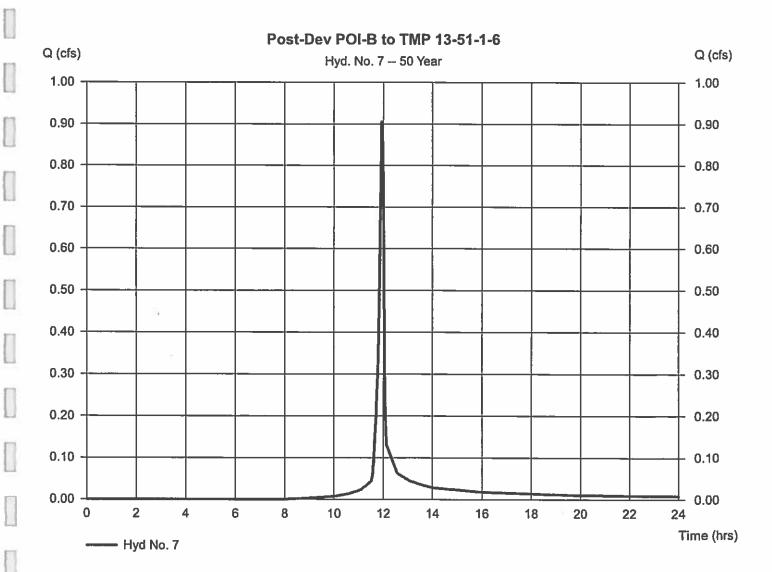
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 50 yrsTime interval = 2 min Drainage area = 0.153 acBasin Slope = 0.0 % Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.905 cfsTime to peak = 11.93 hrs Hyd. volume = 1,835 cuft Curve number = 74 Hydraulic length = 0 ftTime of conc. (Tc) = 5.00 min Distribution = Type II Shape factor = 484



# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.22

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	40.55	2	728	149,176	****		*****	Pre-Dev POI-A
2	SCS Runoff	9.618	2	726	33,286			****	Pre-Dev POI-B to TMP 13-51-1-6
3	SCS Runoff	96.24	2	718	241,937			******	Post-Dev to Basin
4	Reservoir	5.810	2	768	222,119	3	15.73	156,968	Lined Basin
5	SCS Runoff	10.92	2	728	40,084				Post-Dev to Bypass Basin
6	Combine	14.75	2	728	262,203	4, 5			Post-Dev POI-A
7	SCS Runoff	1.078	2	716	2,196				Post-Dev POI-B to TMP 13-51-1-6
	on Recycling.	Dow			Return P	eriod: 100	Year	Wednesday	y, Apr 17, 2019

Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 1

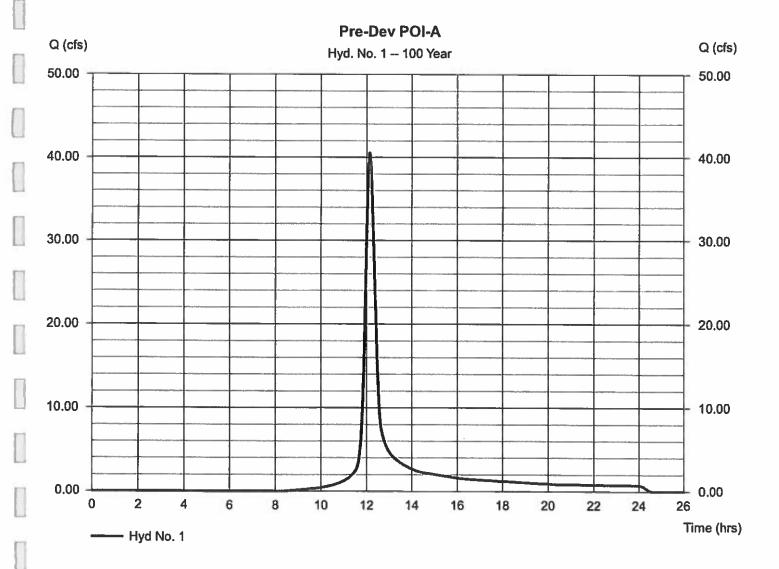
Pre-Dev POI-A

= SCS Runoff Hydrograph type Storm frequency = 100 yrsTime interval = 2 min Drainage area = 11.029 ac Basin Slope = 0.0 %Tc method = TR55 Total precip. = 7.20 inStorm duration = 24 hrs

Peak discharge = 40.55 cfs
Time to peak = 12.13 hrs
Hyd. volume = 149,176 cuft
Curve number = 70
Hydraulic length = 0 ft
Time of conc. (Tc) = 26.80 min
Distribution = Type II

= 484

Shape factor



Hydrafiow Hydrographs by Intelisoive v9.22

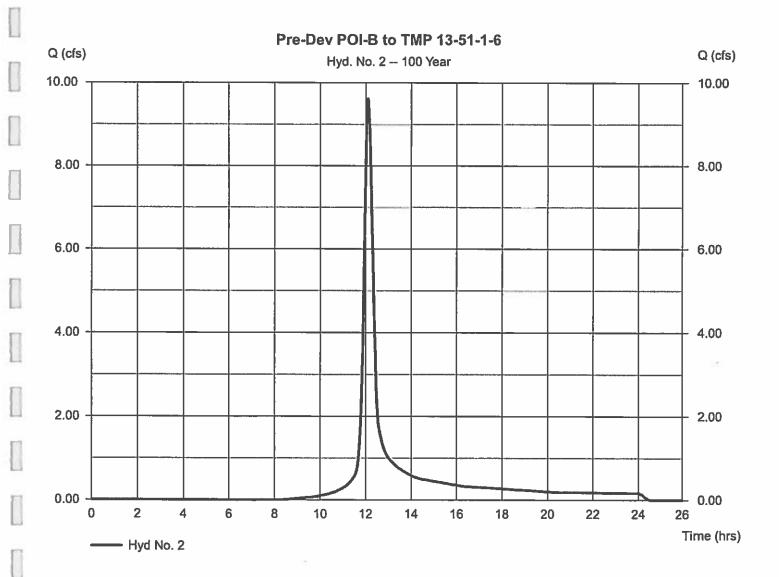
Wednesday, Apr 17, 2019

#### Hyd. No. 2

Pre-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 2.380 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 7.20 inStorm duration = 24 hrs

= 9.618 cfsPeak discharge Time to peak = 12.10 hrs Hyd. volume = 33,286 cuft Curve number = 70 Hydraulic length = 0 ftTime of conc. (Tc)  $= 23.10 \, \text{min}$ Distribution = Type II Shape factor = 484



Hydraflow Hydrographs by Intelisoive v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 3

Post-Dev to Basin

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 10.660 ac Basin Slope = 0.0 % Tc method = USER Total precip. = 7.20 inStorm duration = 24 hrs

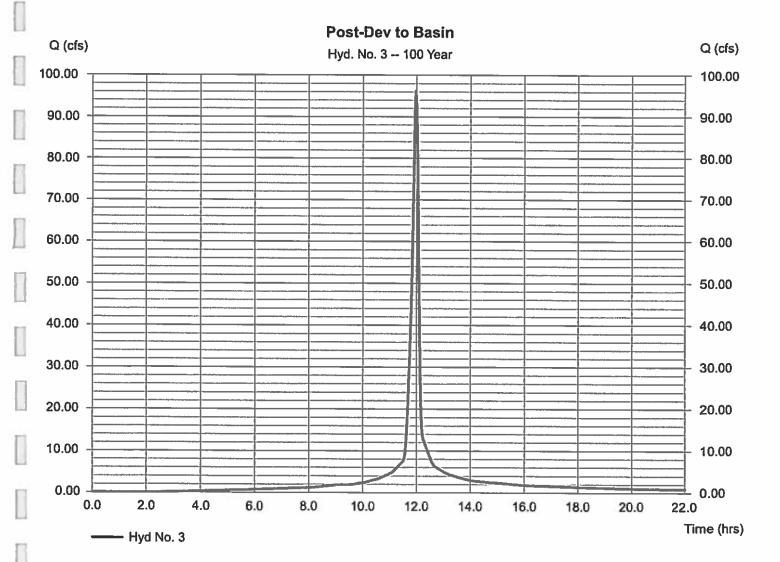
Peak discharge = 96.24 cfs
Time to peak = 11.97 hrs
Hyd. volume = 241,937 cuft
Curve number = 92
Hydraulic length = 0 ft
Time of conc. (Tc) = 8.00 min

= Type Ii

= 484

Distribution

Shape factor



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 4

Lined Basin

Hydrograph type = Reservoir Storm frequency = 100 yrs Time interval = 2 min

Inflow hyd. No. = 3 - Post-Dev to Basin

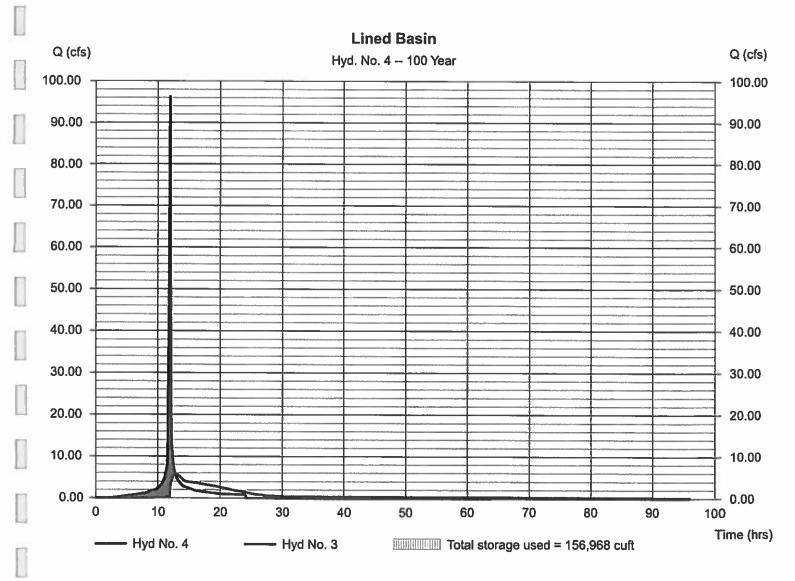
Reservoir name = Lined Basin

Peak discharge = 5.810 cfs Time to peak = 12.80 hrs Hyd. volume = 222,119 cuft

Max. Elevation = 15.73 ft

Max. Storage = 156,968 cuft

Storage Indication method used.



Hydraflow Hydrographs by Intelisolve v9.22

Wednesday, Apr 17, 2019

#### Hyd. No. 5

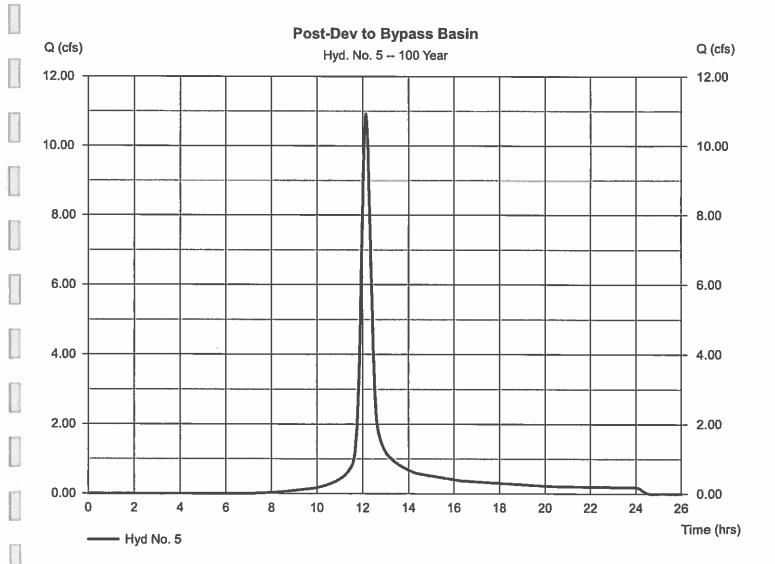
Post-Dev to Bypass Basin

Hydrograph type = SCS Runoff Storm frequency = 100 yrs Time interval = 2 min Drainage area = 2.593 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 7.20 inStorm duration = 24 hrs

Peak discharge = 10.92 cfs
Time to peak = 12.13 hrs
Hyd. volume = 40,084 cuft
Curve number = 75
Hydraulic length = 0 ft
Time of conc. (Tc) = 23.77 min
Distribution = Type II

= 484

Shape factor



Hydraflow Hydrographs by Intelisolve v9.22

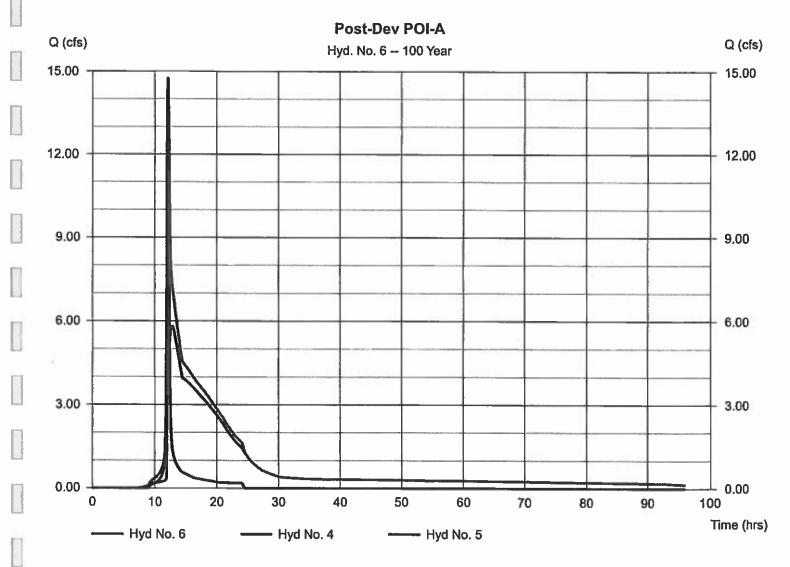
Wednesday, Apr 17, 2019

Hyd. No. 6

Post-Dev POI-A

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 2 min
Inflow hyds. = 4, 5

Peak discharge = 14.75 cfs Time to peak = 12.13 hrs Hyd. volume = 262,203 cuft Contrib. drain. area = 2.593 ac



Hydraflow Hydrographs by Intelisolve v9.22

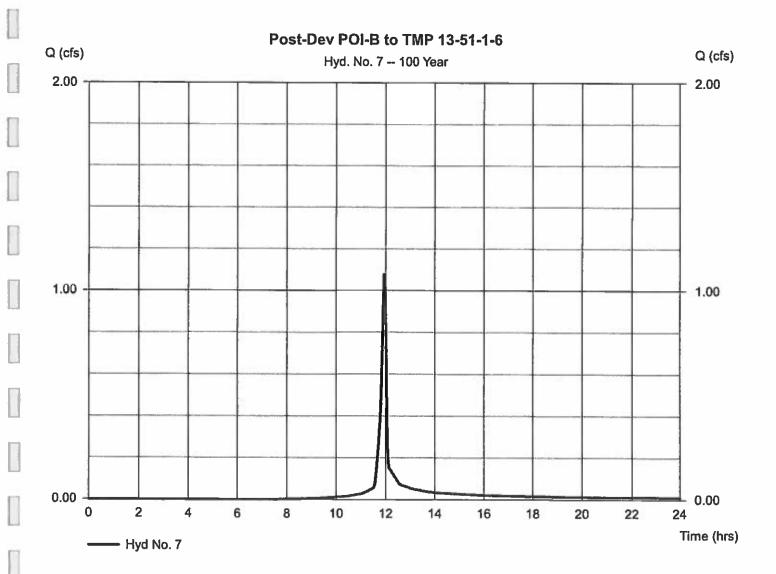
Wednesday, Apr 17, 2019

#### Hyd. No. 7

Post-Dev POI-B to TMP 13-51-1-6

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min = 0.153 acDrainage area Basin Slope = 0.0 %Tc method = USER Total precip. = 7.20 inStorm duration = 24 hrs

Peak discharge = 1.078 cfsTime to peak  $= 11.93 \, hrs$ Hyd. volume = 2,196 cuft Curve number = 74 Hydraulic length = 0 ftTime of conc. (Tc)  $= 5.00 \, \text{min}$ Distribution = Type II Shape factor = 484





**Elcon Recycling** 

**Project Number** 

12-07083

Condition

Post-Development

INL-1										
A	\rea =	22,097	0.51							
Description	С	SF	Α	CxA						
Impervious	0.95	16,290	0.37	0.36						
Grass	0.35	5,807	0.13	0.05						
Forest	0.25	0	0.00	0.00						
TOTAL		22,097	0.51	0.40						
			RC	0.79						

INL-2									
Area = 15,348 0.35									
Description	С	SF	Α	CxA					
Impervious	0.95	15,348	0.35	0.33					
Grass	0.35	0	0.00	0.00					
Forest	0.25	0	0.00	0.00					
TOTAL		15,348	0.35	0.33					
			RC	0.95					

INL-3									
	Area =								
Description	C	SF	Α	CxA					
Impervious	0.95	1,324	0.03	0.03					
Grass	0.35	0	0.00	0.00					
Forest	0.25	0	0.00	0.00					
TOTAL 1,324 0.03									
			RC	0.95					

INL-4									
Α	rea =	8,456	0.19						
Description	С	SF	Α	CxA					
Impervious	0.95	8,456	0.19	0.18					
Grass	0.35	0	0.00	0.00					
Forest	0.25	0	0.00	0.00					
TOTAL	0.19	0.18							
			RC	0.95					

INL-5									
Area = 27,953 0.64									
Description	С	SF	Α	C×A					
Impervious	0.95	23,032	0.53	0.50					
Grass	0.35	4,921	0.11	0.04					
Forest	0.25	0	0.00	0.00					
TOTAL		27,953	0.64	0.54					
			RC	0.84					

INL-6							
Area = 16,482 0.38							
Description	С	SF	Α	C×A			
Impervious	0.95	12,297	0.28	0.27			
Grass	0.35	4,185	0.10	0.03			
Forest	0.25	0	0.00	0.00			
TOTAL		16,482	0.38	0.30			
	0.80						

INL-7									
Α	rea =	17,695	0.41						
Description	С	SF	Α	CxA					
Impervious	0.95	10,482	0.24	0.23					
Grass	0.35	7,213	0.17	0.06					
Forest	0.25	0	0.00	0.00					
TOTAL		17,695	0.41	0.29					
			RC	0570					

INL-8									
Α	rea =	9,960	0.23						
Description	С	SF	Α	CxA					
Impervious	0.95	6,940	0.16	0.15					
Grass	0.35	3,020	0.07	0.02					
Forest	0.25	0	0.00	0.00					
TOTAL		9,960	0.23	0.18					
			RC	0.77					

Elcon Recycling

Project Number

12-07083

Condition

Post-Development

ALACK BERNELS INL-9									
Area = 8,971 0.21									
Description	С	SF	Α	CxA					
Impervious	0.95	6,775	0.16	0.15					
Grass	0.35	2,196	0.05	0.02					
Forest	0.25	0	0.00	0.00					
TOTAL 8,971 0.21									
			RC	0.80					

IÑL-10					
Α	rea =	5,179	0.12		
Description	С	SF	Α	CxA	
Impervious	0.95	4,037	0.09	0.09	
Grass	0.35	1,142	0.03	0.01	
Forest	0.25	0	0.00	0.00	
TOTAL		5,179	0.12	0.10	
	0.82				

INL-11					
,	Area =	13,064	0.30		
Description	С	SF	Α	CxA	
Impervious	0.95	9,666	0.22	0.21	
Grass	0.35	3,398	0.08	0.03	
Forest	0.25	0	0.00	0.00	
TOTAL		13,064	0.30	0.24	
			RC	0,79	

INL-12					
A	rea =	24,299	0.56		
Description	С	SF	Α	CxA	
Impervious	0.95	23,181	0.53	0.51	
Grass	0.35	1,118	0.03	0.01	
Forest	0.25	0	0.00	0.00	
TOTAL		24,299	0.56	0.51	
	0.92				

INL-13					
	Area =	15,224	0.35		
Description	С	SF	Α	CxA	
Impervious	0.95	15,071	0.35	0.33	
Grass	0.35	153	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		15,224	0.35	0.33	
RC					

TD-1					
A	rea =	2,201	0.05		
Description	С	SF	Α	CxA	
Impervious	0.95	2,201	0.05	0.05	
Grass	0.35	0	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		2,201	0.05	0.05	
RC					

TD-2					
Α					
Description	С	SF	Α	CxA	
Impervious	0.95	9,582	0.22	0.21	
Grass	0.35	0	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		9,582	0.22	0.21	
	നള്				

Elcon Recycling

Project Number

12-07083

Condition

Post-Development

TD-3					
P	\rea =	8,561	0.20		
Description	С	SF	Α	CxA	
Impervious	0.95	6,664	0.15	0.15	
Grass	0.35	1,897	0.04	0.02	
Forest	0.25	0	0.00	0.00	
TOTAL		8,561	0.20	0.16	
-			RC	0,82	

.AD-1					
Α	rea =	13,266	0.30		
Description	С	SF	Α	CxA	
Impervious	0.95	13,266	0.30	0.29	
Grass	0.35	0	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		13,266	0.30	0.29	
	0.05				

AD-2					
Area = 12,872 0.30					
Description	С	SF	Α	CxA	
Impervious	0.95	12,872	0.30	0.28	
Grass	0.35	0	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		12,872	0.30	0.28	
	RC				

AD-3					
Α	rea =	9,176	0.21		
Description	С	SF	Α	CxA	
Impervious	0.95	9,176	0.21	0.20	
Grass	0.35	0	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		9,176	0.21	0.20	
	0.95				

AD-4					
Α	rea =	9,109	0.21		
Description	С	SF	Α	C×A	
Impervious	0.95	9,109	0.21	0.20	
Grass	0.35	0	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		9,109	0.21	0.20	
RC					

AD-5					
Α	rea =	23,459	0.54		
Description	С	SF	Α	CxA	
Impervious	0.95	23,459	0.54	0.51	
Grass	0.35	0	0.00	0.00	
Forest	0.25	0	0.00	0.00	
TOTAL		23,459	0.54	0.51	
	0.95				

	AD-	6		
	Area =	35,263	0.81	
Description	С	SF	Α	CxA
Impervious	0.95	35,263	0.81	0.77
Grass	0.35	0	0.00	0.00
Forest	0.25	0	0.00	0.00
TOTAL		35,263	0.81	0.77
			RC	0.95

		D-7		
Α	rea =	2,637	0.06	
Description	С	SF	Α	CxA
Impervious	0.95	2,637	0.06	0.06
Grass	0.35	0	0.00	0.00
Forest	0.25	o	0.00	0.00
TOTAL		2,637	0.06	0.06
	-		RC	0.95

Elcon Recycling

**Project Number** 

12-07083

Condition

Post-Development

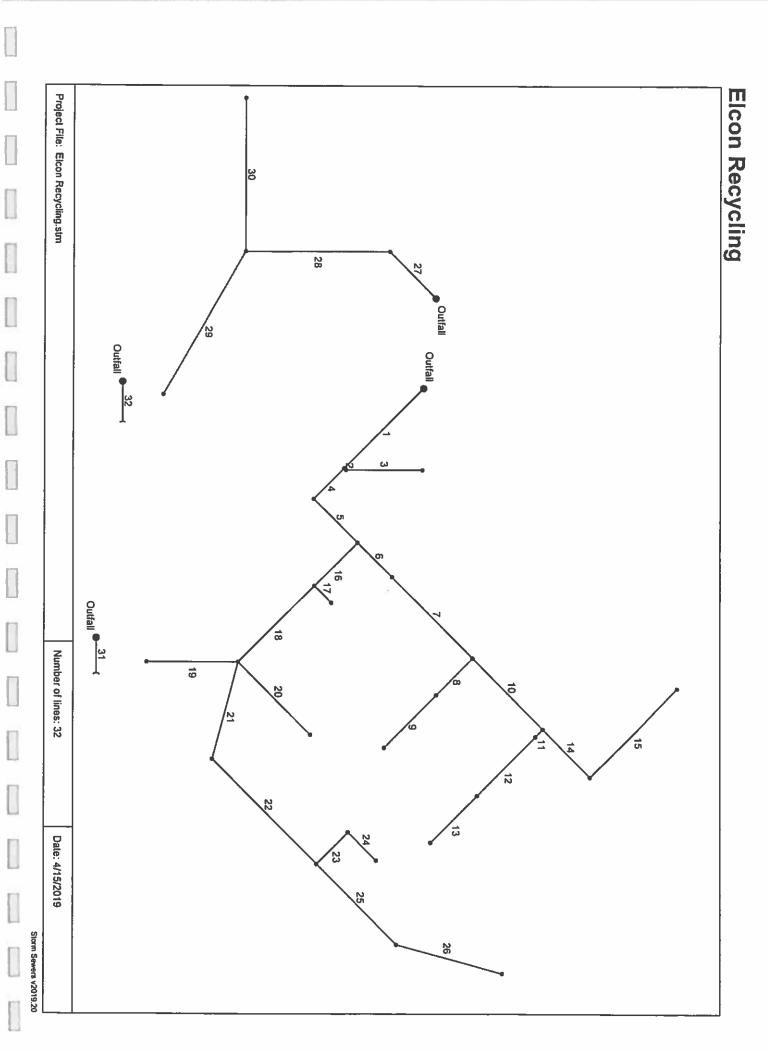
	AD-	8		
	Area =	8,062	0.19	
Description	С	SF	Α	CxA
Impervious	0.95	8,062	0.19	0.18
Grass	0.35	0	0.00	0.00
Forest	0.25	0	0.00	0.00
TOTAL		8,062	0.19	0.18
			RC	0.95

Pr	e-Dev	HW-1		
A	геа =	819	0.019	
Description	С	SF	Α	CxA
Impervious	0.95	0	0.00	0.00
Grass	0.35	819	0.02	0.01
Forest	0.25	0	0.00	0.00
TOTAL		819	0.02	0.01
			RC	0.85

	Pre-D	ev HW-2		1148
А	rea =	45,486	1.044	
Description	С	SF	Α	CxA
Impervious	0.95	0	0.00	0.00
Grass	0.35	45,486	1.04	0.37
Forest	0.25	0	0.00	0.00
TOTAL		45,486	1.04	0.37
			RC	0.35

Po	st-Dev	HW-1		
Α	rea =	613	0.014	
Description	С	SF	Α	CxA
Impervious	0.95	0	0.00	0.00
Grass	0.35	613	0.01	0.00
Forest	0.25	0	0.00	0.00
TOTAL		613	0.01	0.00
			RC	0.35

	Post-L	ev HW-2	2	
Α	rea =	39,818	0.914	
Description	С	SF	Α	CxA
Impervious	0.95	0	0.00	0.00
Grass	0.35	39,818	0.91	0.32
Forest	0.25	0	0.00	0.00
TOTAL		39,818	0.91	0.32
	33		RC	0.35



0.06 20.97 22 Gra 0.02 21.04 23 Gra 0.02 Run Date: 4/15/2019	Number of lines: 32										
20.97	_	Nimber							•	Elcon Recycling	Elcon F
20.97	21.01* 0.4	20.99*	0.540	19.60	19.33	50.000	Ω̈́	5	1,48	AD-8 to AD-7	24
20.70	20.92* 0.1	20.87*	0,500	19.16	18.88	56,000	ξ	15	1.90	AD-7 to INL-9	23
1	20.51* 0.24	19.99*	0.503	18.71	17.78	185.000	ξi.	18	5.61	INL-9 to INL-8	22
0.30 19.92 18	19.61* 0.:	19.09*	0.504	17.61	16.98	125,000	ξ.	18	6.76	INL-8 to STMH-4	21
/a 19.92 i 18	19.67 n/a	19.17	1.422	19.15	17.33	128.000	ξ.	15	1.71	TD-2 to STMH-4	20
0.00 19.20 18	19.20* 0.1	19.19*	0.500	17.90	17.33	114,000	ਨੂੰ	15	0.39	TD-1 to STMH-4	19
0.10 19.09 16	18,99* 0.	18.82*	0.504	16.81	16.13	135.000	ਹੁ	24	8.06	STMH-4 to INL-7	8
0.20 19.08 16	18.89* 0.3	18.78*	0.500	16.28	16.13	30.000	į. Ωį	18	6.31	AD-6 to INL-7	17
0.22 18.78 5	18.56* 0.3	18.46*	0.506	15,96	15,57	77.000	Ω <sub>i</sub>	30	15.00	INL-7 to STMH-3	6
0.06 21.85 14	21.78* 0.1	21.55*	0.500	19.11	18.33	156.000	Ω;	15	2,49	INL-6 to INL-5	15
0.33 21.40 10	21.07* 0.:	20.73*	0.500	18.16	17.74	84,000	ς;	18	6.62	INL-5 to INL-4	14
0.18 21.91 12	21.73* 0.	21.38*	0.542	19.15	18.70	83.000	ξi.	15	4.21	AD-5 to AD-4	13
0.08 21.38 11	21.29* 0.0	20.98*	0.529	18.53	17.98	104.000	ξi,	18	5.77	AD-4 to AD-3	12
0.13 20.88 10	20.75* 0.	20.69*	0.538	17.81	17.74	13.000	ξ	18	7.26	AD-3 to INL-4	=
0.54 20.60 7	20.06* 0.	19.51*	0.504	17.57	16.94	125.000	ਹੂੰ ਹ	24	15,05	INL-4 to INL-3	10
0.06 20.32 8	20.26* 0.0	20.14*	0.505	17.91	17.44	93.000	ਹੁੰ	15	2.34	AD-2 to AD-1	9
0.11 19.98 7	19.87* 0.	19.55*	0,508	17.27	16.94	65.000	Ç	15	4.55	AD-1 to INL-3	O2
0.38 19.51 6	19.12 0.	18.83	0.500	16.77	16.05	144.000	Č.	30	19.45	INL-3 to INL-2	7
0.15 18.78 5	18.63* 0.	18.46*	0.508	15.88	15.57	61,000	ç	30	21.60	INL-2 to STMH-3	6
/a 18.46 i 4	17.29 n/a	17.88	0.513	15.40	15.00	78.000	č.	36	33.87	STMH-3 to WQ FILTER	Ch
0.36 17.88 1	17.51 0.:	17.40	0.500	14.65	14,38	54,000	ਪੂ	36	33.65	WQ FILTER to STMH-1	4
0.11 17.85 2	17.74* 0.	17.49*	0.500	15.05	14.57	96,000	č.	15	3,30	INL-1 to STMH-2	ω
0.08 17.49 1	17.40° 0.1	17.40*	0.667	14.40	14.38	3.000	Ĉ.	Ġ	3,24	STMH-2 to STMH-1	N
/a 17.40 i End	16.17 n/a	15.72	0.504	14.21	13.50	141.000	ç	36	36.14	STMH-1 to EW-1	
Minor HGL Dns loss Junct Lina (ft) (ft) No.	HGL Min (ft)	HGL Down	Line Slope (%)	(ft)	Invert EL Dn (ft)	Line length (ft)	Line	Line Size (in)	Flow rate (cfs)	Line (D	Line No.
		1			1	-	7	Report		Sewer Summary	Storm S

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# **Storm Sewer Summary Report**

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NOTES	Elcon	32	31	30	29	28	27	26	25	Line No.
NOTES: Return period = 100 Yrs.; *Surcharged (HGL above crown).; i - Inlet control	Elcon Recycling	HW-2 to EW-5	HW-1 to EW-4	INL-13 to INL-12	TD-3 to INL-12	INL-12 to STMH-5	STMH-5 to EW-2	INL-11 to INL-10	JNL-10 to INL-9	Line ID
charged (HC		1.84	0.09	2.70	1.34	7.50	7.36	1,94	2.63	Flow rate (cfs)
L above crow		24	15	ċ	σħ	18	18	15	15	Line Size (in)
m). ; i - Inle		압	Ç.	Ç	Ç	읔	Ş.	압	Č.	Line
at control.		50.000	44,000	190.000	205.000	181.000	82.000	138.000	142.000	Line length (ft)
		14.40	17.18	15.45	15.45	14.25	13.65	19.76	18.88	(ft)
		14.75	17.40	16.40	16.50	15.25	14.08	20.45	19.59	(ft) EL Up
		0.700	0.500	0.500	0.512	0.552	0.524	0.500	0.500	Line Slope (%)
	Number of lines: 32	14.87	17.29	16,87	16.87	15.60	14.70	21.16	20.83*	HGL Down (ft)
	lines: 32	15.22	17.53	17.23	17.08	16.42	15.32	21.29	21.07*	(#) Up HGL
		n/a	n/a	0.15	0.09	n/a	n/a	0.08	0.06	Minor loss (ft)
	Run [	15.42 i	17.53 i	17.38	17.17	16.87 i	15.60 i	21.36	21.13	HGL Junct (ft)
	Run Date: 4/15/2019	End	End	28	28	27	End	25	22	Dns Line No.
	2019	OpenHeadwall	OpenHeadwall	Combination	Grate	Combination	Manhole	Combination	Combination	Junction Type

# **Storm Sewer Tabulation**

							í		box	ellip b=	cir e=	100 ; c=	=Yrs. 1ı	n period	4; Retu	00) ^ 1.0	ne + 27.	(Inlet tin	00.36/	NOTES:Intensity = 300.36 / (Inlet time + 27.00) ^ 1.04; Return period =Yrs.	ES:Inte	NO
15/2019	Run Date: 4/15/2019			32	Number of lines: 32	Numbe														ciing	Elcon Recycling	Elco
00   INL-9 to INL-8	00 23,00	23.00	20.51	19.99	18.71	17.78	0.50	18	3.18	7.45	5.61	7.6	7.5	5.0	0.74	0.17	0.80	0.88	0.21	185.000 0.21	21	22
00 INL-8 to STMH-4	70 23.00	1 22.70	19.61	19.09	17.61	16.98	0.50	18	3.83	7.46	6.76	7.4	со Сл	5.0	0.92	0.18	0.77	1.11	0.23	125.000 0.23	18	21
25 TD-2 to STMH-4	70 22.25	7 22.70	19.67	19.17	19.15	17.33	1.42	5	2.47	7.70	1.71	8.2	5.0	5.0	0.21	0.21	0.95	0.22	0.22	128.000 0.22	18	20
00 TD-1 to STMH-4	70 21.00	22.70	19.20	19.19	17.90	17.33	0.50	3	0.32	4.57	0.39	8.2	5.0	5.0	0.05	0.05	0.95	0.05	0.05	114.000 0.05	68	19
70 STMH-4 to INL-7	70 22.70	9 20.70	18.99	18.82	16.81	16.13	0.50	24	2.56	16.05	8.06	6.9	11.0	0.0	1.17	0.00	0.00	1.38	0.00	135.000 0.00	16	18
33 AD-6 to INL-7	70 19.63	9 20.70	18.89	18.78	16.28	16.13	0.50	18	3.57	7.43	6.31	8.2	5.0	5.0	0.77	0.77	0.95	0.81	0.81	30.000	16	17
70   INL-7 to STMH-3	80 20.70	5 21.80	18.56	18.46	15.96	15.57	0.51	30	3.06	29.19	15.00	6.7	11.8	5.0	2.24	0.29	0.71	2.60	0.41	77.000	Ø1	16
21 INL-6 to INL-5	05 22.21	в 22.05	21.78	21.55	19.11	18.33	0.50	15	2.03	4.57	2.49	8.2	نار 0	5.0	0.30	0.30	0.80	0.38	0.38	156.000 0.38	14	亦
)5   INL-5 to INL-4	65 22.05	7 21.65	21.07	20.73	18.16	17.74	0.50	18	3.75	7.43	6.62	7.9	6.3	5.0	0.84	0.54	0.84	1.02	0.64	84.000	10	4
25 AD-5 to AD-4	50 22.25	3 22.50	21.73	21.38	19.15	18.70	0.54	5	3.43	4.75	4.21	8.2	5,0	5.0	0.51	0.51	0.95	0.54	0.54	83.000	12	13
50 AD-4 to AD-3	00 22.50	9 22.00	21.29	20.98	18.53	17.98	0.53	18	3.26	7.64	5.77	8.1	UI A	5.0	0.71	0.20	0.95	0.75	0.21	104.000 0.21	⇉	12
00 AD-3 to INL-4	65 22.00	5 21.65	20.75	20.69	17.81	17.74	0.54	18	4.11	7.71	7.26	8.0	5.9	5,0	0.91	0.20	0.95	0.96	0.21	13.000	10	=======================================
35   INL-4 to INL-3	55 21.65	6 22.55	20.06	19.51	17.57	16,94	0.50	24	4.79	16.06	15.05	7.8	6.6	5.0	1.93	0.18	0.95	2.17	0.19	125.000 0.19	7	10
20 AD-2 to AD-1	00 21.20	6 21.00	20.26	20.14	17.91	17.44	0.51	ij	1.90	4.59	2.34	8.2	5.0	5.0	0.29	0.29	0.95	0.30	0.30	93.000	œ	ဖ
00 AD-1 to INL-3	55 21.00	7 22.55	19.87	19.55	17.27	16.94	0.51	15	3.71	4.60	4.55	8.0	5.8	5.0	0.57	0.29	0.95	0.60	0.30	65.000	7	œ
55   INL-3 to INL-2	95 22.55	2 20.95	19.12	18.83	16.77	16.05	0.50	30	4.01	29.00	19.45	7.7	7.1	5.0	2.53	0.03	0.95	2.80	0.03	144,000 0,03	on	7
95   INL-2 to STMH-3	80 20.95	3 21.80	18.63	18.46	15.88	15.57	0.51	30	4.40	29.24	21.60	7.5	7.7	5.0	2.87	0.33	0.95	3.15	0.35	61.000	Ch	თ
STMH-3 to WQ FI	60 21.80	9 23.60	17.29	17.88	15.40	15.00	0.51	36	6.04	47.76	33.87	6.6	12.2	0.0	5.10	0.00	0.00	5.75	0.00	78.000	4	G
30 WQ FILTER to ST	90 23.60	1 22.90	17.51	17.40	14.65	14.38	0.50	36	4.80	47.16	33.65	6.6	12.4	0.0	5.10	0.00	0.00	5.75	0.00	54.000	_	4
35 INL-1 to STMH-2	85 21.35	4 22.85	17.74	17.49	15.05	14.57	0.50	15	2.69	4.57	3.30	8.20	5.0	5.0	0.40	0.40	0.79	0.51	0.51	96.000	N	ω
85 STMH-2 to STMH	90 22.85	0 22.90	17.40	17.40	14.40	14.38	0.67	15	2.64	5.27	3.24	8.0	Çī.	0.0	0.40	0.00	0.00	0.51	0.00	3.000	_	2
30 STMH-1 to EW-1	00 22.90	7 18.00	16.17	15.72	14.21	13.50	0.50	36	6.92	47.33	36.14	6.6	12.6	0.0	5.50	0.00	0.00	6.26	0.00	141,000	E M	_
	æ	3	€	€	(FE)	(ft)	(%)	(in)	(ft/s)	(cfs)	(cfs)	(in/hr)	(min)	(min)			ŝ	(ac)	(ac)	(35)		
	Пр	Dn	Up	Dn	ф	Da	Slope	Size		=	10	= =	Syst	Inlet	Total	incr		Total	Incr		50	Line
ev Line ID	Grnd / Rim Elev	Gra	Тev	HGL Elev	lev	Invert Elev		Pipe	Vel	Cap	Total	Rain		Tc	Ö	Агеах	Rnoff	rea	Drng Area	Len	Š	Station

Storm Sewers v2019.20

# **Storm Sewer Tabulation**

팂		32	ઞ	30	29	28	27	26	25	24	23		Line	Station
Elcon Recycling		End	E	28	28	27	End	25	22	23	22	-	5 7	9
ycling		50.000		190.0	205.0	181.0		138.0	142.0	50.00	56.00	3		Len
		0.64	44.000 0.03	190.000 0.35	205.000 0.20	181.000 0.56	82.000 0.00	138.000 0.30	142.000 0.12	50.000 0.19	56.000 0.06	(ac)	Incr	D mg
		0.64	0.03	0.35	0.20	1.11	1.11	0.30	0.42	0.19	0.25	(ac)	Total	Drng Area
												(0)		3 27
		0.35	0.35	0.94	0.82	0.92 0	0.00	0.79	0.82	0.95	0.95	_		Rnoff
		0.22	0.01	0.33	0.16	0.52	0.00	0.24	0.10	0.18	0.06		lncr	Area x C
		0.22	0.01	0.33	0.16	1.01	1.01	0.24	0.34	0.18	0.24		Total	
		5.0	5.0	5.0	5.0	5.0	0.0	5.0	5.0	5.0	5.0	(min)	inlet	16
		5.0	5.0	5.0	5,0	8.1	8.8	5.0	5.5	5.0	5.7	(min)	Syst	
		8.2	8.2	8.2	8.2	7.4	7.3	8.2	7.8	8.2	8.0	(in/hr)	=======================================	Rain
		1.84	0.09	2.70	1.34	7.50	7.36	1.94	2.63	1.48	1.90	(cfs)	i	Total
		18.92	4.57	4.57	4.62	7.81	7.60	4.57	4.57	4.75	4.57	(cfs)		- C
		92 3.27	7 1.44	7 2.65	2 1.76	1 4.77			7 2.14	5 1.21		(ft/s)		<u>§</u>
							5.14	1.90			1.55	E) (in)	Size	
		24 0	15	15	15	18	18	15	15	15 0	15	(%)		Pipe
		0.70	0.50	0.50	0.51	0.55	0.52	0.50	0.50	0.54	0.50		Slope	_
Numbe		14.40	17.18	15.45	15.45	14.25	13.65	19.76	18.88	19.33	18.88	Æ	Dn	Invert Elev
Number of lines: 32		14.75	17.40	16.40	16.50	15.25	14.08	20.45	19.59	19.60	19.16	3	q	lev
s: 32												<b>æ</b>	Da	
		14.87	17.29	16.87	16,87	15.60	14.70	21.16	20.83	20.99	20.87			HGL Elev
		15.22	17,53	17.23	17.08	16.42	15.32	21.29	21.07	21.01	20.92	3	d⊓	
2		17.00	18.00	20.40	20.40	22.00	17.75	23.60	23.00	22.45	23.00	Ê	D	Gm
n Date:														Grnd / Rim Elev
Run Date: 4/15/2019		17.00	19.00	19.50	19.60	20.40	22.00	23.55	23.60	23.00	22.45	€	υþ	Elev
019	3	HW-2	HW-1	NL-1	TD-3 I	NL-1	STMH	NL-1	INL-1	AD-8	AD-7			Line ID
		HW-2 to EW-5	HW-1 to EW-4	INL-13 to INL-12	TD-3 to INL-12	INL-12 to STMH-5	STMH-5 to EW-2	INL-11 to INL-10	INL-10 to INL-9	AD-8 to AD-7	AD-7 to INL-9			9
		Ch	4	-12	Ñ	MH-5	W-2	10	6					

NOTES:Intensity = 300.36 / (Inlet time + 27.00) \* 1.04; Return period = Yrs. 100; c = cir e = ellip b = box

